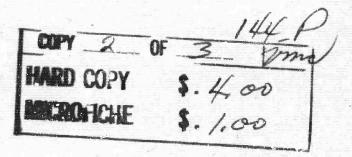
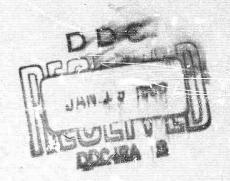
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SCIENTIFIC REPORT

ABSORPTION BY CO₂ BETWEEN 4500 AND 5400 cm⁻¹

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15 December 1964

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ABSTRACT

The absorption by 38 different samples of $\rm CO_2$ in the 4500 - 5400 cm $^{-1}$ (near 2 microns) region has been studied with the use of a spectrometer having a spectral resolution between approximately 0.3 and 1 cm $^{-1}$. Samples of $\rm CO_2$ and $\rm CO_2 + N_2$ were contained in two different absorption cells; one having a maximum path of 933 meters and used at a maximum pressure of 2.5 atm. The other was used at paths as long as 32.9 meters and at pressures as high as 15 atm. Photographs of the spectra of every sample as well as a table of transmittance versus wavenumber are included. Also presented is a table of the integrated absorptance

$$v^{1}$$
 $\left[1 - T(v)\right] dv$

versus ν , where approximately 600 values are tabulated for the largest samples.

ACKNOWLEDGMENT

The authors would like to acknowledge the assistance of several people during the course of this investigation. Mr. Francis Gates performed much of the work in getting the instruments assembled and in reducing the data. Mr. Ronald Steen also helped considerably in digitizing the data. Dr. Byron Edwards provided much assistance in developing the method and the instruments used in digitizing the spectral records. Mr. Ricardo DeCasas wrote the computer program and assisted in all the work connected with the computer.

Dr. William S. Benedict of Johns Hopkins University made many worthwhile suggestions and is responsible for the identification of several new absorption bands. Several helpful discussions with Drs. Louise Gray and Lewis Kaplan of the Jet Propulsion Laboratory are also greatly appreciated.

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FOREWORD

The work reported here is a portion of an extensive investigation of the absorption of infrared radiation by atmospheric gases. Reports similar to this one but dealing with other spectral regions will be published within the next few months. This report does not contain much in the way of analysis of the data, but very detailed results are included in a manner which should be convenient for other workers. We expect to use the data presented here for at least one more report which will deal with the shapes and strengths of many of the earth and other planets.

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SECTION 1

INTRODUCTION AND SUMMARY

The major portion of the absorptio by $\rm CO_2$ in the 4500-5400 cm⁻¹ region (near 2 microns) is due to three combination bands: $2^{1}1^{-1}$ v_3 whose center is at 5099.62 cm⁻¹, $v_1 + 2v_2 + v_3$ at 4977.79 cm⁻¹ and $4v_2 + v_3$ at 4853.28 cm⁻¹. Besides these three bands of medium strength, there are approximately v_0 weaker bands which have been observed in this region, and at certain vavenumbers one or more of them may p duce most of the absorption.

Howard, Burch and Williams have made some quantitative measurements on the absorption in this region, but the spectral resolution of their instrument was low. Courtoy has measured the positions of several hundred absorption lines with very good accuracy and has identified many bands which had not been observed previously; but only limited information about the amount of absorption one might expect from a given sample can be obtained from his results. Weber, Holm and Penner have measured the strengths of the three main bands, but with an accuracy of only ± 20 percent. Breeze and Ferriso have also investigated the effect of changing the temperature on the band strengths. Kuiper has investigated the absorption by large samples; but his measurements were made with only moderate resolution and at pressures of several atmospheres.

Because of the limitations of the previous work, there was still need for data on samples covering wide ranges of pressure and absorber thickness and with resolution sufficiently good that at least some lines from most of the bands could be resolved. The present investigation was undertaken for the purpose of obtaining these data. The long absorption call with possible paths as great as 933 meters has enabled us to study

samples having very large absorber thickness at pressures which are not so great as to smooth out the structure in the band. The short absorption cell has also made it possible to investigate samples at higher pressures in order that band strengths can be measured easily.

From the results presented in this report one should be able to determine the strengths of nearly every band of any significance in this region. The widths of most of the lines can also be determined from "curves of growth" of the average absorptance over relatively narrow intervals. Once the strengths and widths of the lines have been found, the absorptance at any wavenumber can be calculated for a great variety of samples, even though they are quite different from any of the samples studied. This is true, even for samples having non-uniform temperature and pressure.

Because of the long paths which are possible with the long absorption cell, we have been able to observe and identify five new CO₂ bands in this region which have not been reported previously. Approximate strengths of these as well as the three major bands have been determined and are tabulated in Section 3.

Spectra of 38 samples covering a wide range of pressures and path lengths have been reproduced and digitized. The reproduced spectra are shown in Section 5 and a table of transmittance $T(\nu)$ versus wavenumber ν is presented in Section 6. Section 7 contains a table of

$$\int_{v^{1}}^{v} \left[1 - T(v)\right] dv,$$

the integrated absorptance versus wavenumber; ν^l is on the low wavenumber side of the region considered for a given sample, and tabulations are made for nearly 600 different values of ν for the largest samples.

Detailed descritpions of the two absorption cells used and of the digitizing apparatus are given in Appendices A, B, and C.

SECTION 2

EXPERIMENTAL METHODS

2.1 GAS SAMPLING

Samples of CO_2 and $\mathrm{CO}_2 + \mathrm{N}_2$ were contained in two different absorption cells which are described in detail in Appendices A and B. The longer cell has a base length of approximately 30 meters and was used at as many as 32 passes, giving a total path length of 933 meters. This cell is approximately 0.9 meters in diameter and can be evacuated to less than 1 micron of Hg or pressurized to as much as 2.5 atmospheres. The shorter cell has a base length of approximately 1 meter and was used at as many as 32 passes. It also can be evacuated and pressurized to as much as 15 atmospheres.

The ${\rm CO}_2$ was taken from the vapor in a dewar which contained both liquid and vapor. It was maintained at a temperature less than about $-20^{\circ}{\rm C}$, so that the pressure never exceeded approximately 300 psig. There was found to be considerably less water in the sample if it were drawn from the vapor over the liquid rather than allowing the liquid to be drawn off and to evaporate into the cell. It appeared as though most of the water in the ${\rm CO}_2$ container was trapped in the liquid ${\rm CO}_2$; and if the liquid was drawn off the ${\rm H}_2{\rm O}$ was allowed to enter the absorption cell. Of course, as the vapor was drawn off the pressure, and thus the temperature, in the dewar dropped considerably and the filling rate decreased. When the pressure dropped below about 50 psig, the valves were closed and the dewar was allowed to warm up. Approximately two days were required to fill the large absorption cell to 2.5 atmospheres from two dewars of ${\rm CO}_2$.

The cell could have been filled in much less time by drawing off the liquid ${\rm CO_2}$ rather than the vapor, but the slower technique was chosen because of the drier samples which could be obtained. The amount of ${\rm H_2O}$ in the ${\rm N_2}$ was much less than that in the ${\rm CO_2}$ therefore, it was not necessary to take extreme care to reduce the amount of ${\rm H_2O}$ put into the sample with the ${\rm N_2}$ which was drawn off as a liquid into a heat exchanger where it evaporated and entered the cell.

Before introducing a sample into the cell, the cell was pumped for several hours in order to get rid of most of the H₂O which was adsorbed on the walls. This can be very important, depending on the previous sample in the cell. Even after using this much care, the absorption by traces of H₂O in the sample was bothersome at some wavenumbers.

 ${\rm CO}_2$ + ${\rm N}_2$ mixtures were mixed in the cell; ${\rm CO}_2$ was added to the desired pressure, ${\rm N}_2$ was then added and the mixing was accomplished by fans inside the absorption cells. No attempt was made to change the relative abundances of the different isotopes of C or O in the samples studied.

Sample pressures less than approximately 0.06 atm were measured with a U-tube oil manometer, and a U-tube H $_{\rm g}$ manometer was used for pressures in the range 0.06 < P < 2 atm. All pressures > 2 atm were measured with a bourdon-type gauge.

Since CO₂ varies significantly from a perfect gas at some of the higher pressures used in this investigation, it was necessary to account for the Van der Waals' forces giving ise to the deviation from the perfect gas. In calculating the absorber thickness u, the following equation was used:

$$u = W p L \frac{273}{296}$$
 (atm cm) STP. (1)

L is the path length in centimeters,

p is the partial pressure of CO₂ in atmospheres,

273/296 accounts for the difference in density between room temperature and standard temperature,

W is a correction term which accounts for the Van der Waels' forces and is given adequately for the pressures used in this investigation by

$$W = 1.00 + 0.0047 p. (2)$$

All measurements were made with the samples at room temperature, approximately $296^{\circ}K$.

In order to relate the pressure of a sample to the half-width of the absorption lines, it is necessary to account for the different broadening abilities of CO_2 and N_2 when dealing with mixtures of these two gases. Burch, Gryvnak and Williams have used an equivalent pressure P_{e} given by

$$P_e = 1.3 p + (P - p)$$
 (3)

where P is the total pressure. It is noted that the equivalent pressure approaches the total pressure for a very dilute mixture of $\rm CO_2$ in $\rm N_2$.

Since the simple classical theory predicts that the half-width of a line is proportional to the density of molecules, equation (3) should probably be modified to account for Van der Waals' forces which cause the density to increase faster than the pressure. The adjustment can be made by modifying (3) in the following way:

$$P_e = 1.3 W p + (P - p).$$
 (3')

The factor 1.3 is not valid in all portions of the spectrum, but it has been found to represent satisfactorily the different broadening abilities throughout most portions of the band not too distant from the absorption lines producing the absorption. Winters, Silverman and Benedict' have found, for example, that the self-broadening factor should be considerably greater than 1.3 when dealing with regions such as that on the high wavenumber side of the 2350 ${\rm cm}^{-1}$ ${\rm CO}_2$ band, where all of the absorption is due to the wings of very strong lines whose centers are several cm⁻¹ away. This results from the fact that the shape of a selfbroadened line several cm-1 from the line center is quite different from that of a nitrogen-broadened line. Although (3') does not give an accurate representation of an equivalent pressure which is proportional to the line half-width for all regions in the spectrum, it is adequate in most cases and serves to simplify the analysis of the data. As more accurate methods of accounting for the self-broadening are found a better value for equivalent pressure for the samples in any spectral region can be obtained.

2.2 RECORDING AND CALIBRATION OF SPECTRA

The spectrometer is "home made" and was contained in a tank which could be evacuated to essentially eliminate absorption due to atmospheric gases outside of the absorption cell. The spectrometer tank, as well as another tank containing the radiation source and chopper, were connected to the absorption cell by means of flexible bellows so that all of the optical path external to the absorption cell could be evacuated.

The spectrometer is of the Ebert type with the main mirror having a 75 cm focal length. It utilized a small grating having a ruled area 64 x 64 mm with 600 lines/mm and blazed at 1.6 microns. The grating was used in the first order and a Ge filter eliminated overlapping orders of shorter wavelength. A PbS cell cooled with liquid nitrogen was used as the detector. It was not necessary to cool the detector below dry ice temperature for operation in this wavelength region, but the dewar was designed to hold the liquid nitrogen for use at longer wavelengths. Cooling by liquid nitrogen was, therefore, more convenient and was used since the signal-to-noise ratio was approximately the same at both temperatures. Three different resolution schedules were used in recording the spectra; the approximate spectral slitwidths for each schedule at three different wavenumbers are given in Table 2-1.

TABLE 2-1
RESOLUTION SCHEDULES

		ectral Slitwidth (cm	⁻¹)
(cm ⁻¹)	Schedule A	Schedule B	Schedule C
(сш.)			
4600	0.30	0.39	0.54
5000	0.35	0.50	0.70
5400	0.41	0.62	0.86

Resolution Schedule A was used in several regions of the spectrum to resolve closely spaced lines; but because of the small signal available while using this schedule, considerable time was required to scan a portion of the spectrum. Therefore, Schedule B

which represents a compromise between resolution and scanning time was used for the majority of the data. Schedule C was used for some spectra of samples at several passes of the absorption cell for which the signal was low.

Background curves were obtained with the sample cell evacuated for each number of passes for which measurements were obtained. The background curve was different for different numbers of passes since the reflectivity of the mirrors in the multiple-pass optics varies with wavenumber. The appropriate background curve which represents 100 percent transmittance was then fitted to each spectrum and traced on it. All the sample spectra extended beyond the region of absorption on both ends of the band so that dependable "tie-points" between a spectrum and its background could be established. The transmittance was determined from the ratio of the deflection of the sample spectrum to that of the background curve at the same wavenumber. Each spectrum was digitized, with the information put on IBM cards by the technique which is described in considerable detail in Appendix C.

Most of the points used in the wavenumber calibration were obtained from the ${\rm CO}_2$ lines of the bands being studied since the positions of many of them have been determined with very good accuracy by ${\rm Courtoy}^2$. The lines of a few other bands which have not been measured or calculated by ${\rm Courtoy}$ can be determined from the values of the molecular constants provided by him. The wavenumbers of several lines in the ${\rm CO}_2$ band of ${\rm CO}_2$ which was omitted by ${\rm Courtoy}$ have been measured by ${\rm Diaz}^8$; his values were used for calibration in the region of this band. H₂O lines whose positions are well known were also used as standards in certain parts of the spectrum.

Lines separated by an average of about 10 cm⁻¹ were used in calibrating each spectrum; it was assumed that each spectrum was linear between the calibration points. The absorption lines used as standards are summarized in Table 5-1, and each of the lines is indicated in the spectra shown in Section 5.

SECTION 3

DISCUSSION OF ABSORPTION BANDS

3.1 IDENTIFICATION OF ABSORPTION BANDS

which absorb appreciably in this region are listed in Table 3-1. ν_0 is the wavenumber of the center of the band for the species and the transition indicated. Portions of all but five or six of these absorption bands have been observed with good resolution in the very extensive work of Courtoy 2 . By using samples in which the abundances of some of the less common isotopes were enhanced, Courtoy was able to observe absorption lines which would otherwise be hidden by the lines of the more common isotopes. Several of the absorption bands of these rarer isotopes do not contribute significantly to the absorption by samples having the natural abundance of each isotope.

Most of Courtoy's measurements dealt with the determination of the positions of the absorption lines with very good accuracy, but only limited information about the strengths of the lines can be obtained from his results. Kniper has measured the absorption by large samples for about 20 absorption bands in this region and correlated some of them with bands observed in the spectrum of Venus. Kniper also observed some absorption at about $4505~\rm cm^{-1}$ which he attributed to the 002-000 transition of $C^{13}0^{16}0^{18}$. We were not able to observe this band for the largest sample used, which was at a pressure of 2.5 atm and a path length of 933 meters. In our experiment the noise is approximately three or four percent of the signal in this portion of the spectrum when operating at the maximum path length; therefore, it is possible that the absorptance near the middle of a band in this region could be as much as 0.02 or 0.03 without being detected by us. Unfortunately, only two or three spectra of very large samples were obtained by us in this region

TABLE 3-1 CO_2 BANDS BETWEEN 4500 and 5400 cm⁻¹

o cm-1	Transition	Species	o cm-1	Transition	Species
4591.0 ^a 4639.53 ^c 4673.635 4685.715 4687.75 ^a 4692.120 4708.477 4748.012 4768.49 4790.520 4791.208 4807.652 4814.530 4839.704 4853.578	$15^{1}0^{b}$ $00^{0}2$ $0c^{2}1 \leftarrow 02^{2}0$ $06^{0}1 \leftarrow 02^{0}0$ $06^{0}1 \leftarrow 10^{0}0$ $04^{0}1$ $05^{1}1 \leftarrow 01^{1}0$ $06^{0}1 \leftarrow 02^{0}0$ $20^{0}1$ $05^{1}1 \leftarrow 01^{1}0$ $12^{0}1$ $14^{0}1 \leftarrow 10^{0}0$ $04^{0}1$	$\begin{array}{c} c^{12}o_{2}^{16} \\ c^{12}o_{2}^{16}o_{1}^{18} \\ c^{13}o_{2}^{16} \\ c^{13}o_{2}^{16} \\ c^{12}o_{2}^{16} \\ c^{13}o_{2}^{16} \\ c^{13}o_{2}^{16} \\ c^{13}o_{2}^{16} \\ c^{12}o_{2}^{16} \\ c^{12}o_{2}^{16} \\ c^{12}o_{2}^{16} \\ c^{13}o_{2}^{16}o_{1}^{18} \\ c^{12}o_{2}^{16} \\ c^{12}o_{2}^{16} \\ c^{12}o_{2}^{16} \\ c^{12}o_{2}^{16} \\ c^{12}o_{2}^{16} \end{array}$	4942.484 4953.327 4959.635 4965.337 4976.095 4977.793 4991.309 4993.520 5013.730 5028.730 5042.538 5062.394 5099.619 5123.170 5139.400	$ \begin{array}{c} 14^{0}1 \leftarrow 02^{0}0 \\ 14^{2}1 \leftarrow 02^{2}0 \\ 22^{0}1 \leftarrow 10^{0}0 \\ 13^{1}1 \leftarrow 01^{1}0 \\ 22^{0}1 \leftarrow 02^{0}0 \\ 12^{0}1 \\ 20^{0}1 \\ 30^{0}1 \leftarrow 10^{0}0 \\ 21^{1}1 \leftarrow 01^{1}0 \\ 22^{2}1 \leftarrow 02^{2}0 \\ 04^{0}1 \\ 22^{0}1 \leftarrow 02^{0}0 \\ 20^{0}1 \\ 21^{1}1 \leftarrow 01^{1}0 \\ 22^{2}1 \leftarrow 02^{2}0 \end{array} $	$\begin{array}{c} c^{12}c_{2}^{16} \\ c^{12}c_{2}^{16} \\ c^{12}c_{2}^{16} \\ c^{12}c_{2}^{16} \\ c^{12}c_{2}^{16} \\ c^{13}c_{2}^{16} \\ c^{13}c_{2}^{16} \\ c^{13}c_{2}^{16} \\ c^{13}c_{2}^{16} \\ c^{13}c_{2}^{16} \\ c^{12}c_{2}^{16}c_{2}^{18} \\ c^{12}c_{2}^{16} \end{array}$
4853.745 4858.100 4871.408 4871.860 4887.348 4904.820 4924.990	$ \begin{array}{c} 14^{0} & 1 & 1 & 1 & 1 & 1 & 1 \\ 14^{0} & 1 & 1 & 1 & 1 & 1 \\ 14^{0} & 1 & 1 & 1 & 1 & 1 \\ 13^{1} & 1 & 1 & 1 & 1 & 1 \\ 22^{0} & 1 & 1 & 1 & 1 & 1 \\ 12^{0} & 1 & 1 & 1 & 1 & 1 \\ 20^{0} & 1 & 1 & 1 & 1 & 1 \\ \end{array} $	$\begin{array}{c} c^{13}o_{2}^{16} \\ c^{13}o_{2}^{16} \\ c^{13}o_{2}^{16} \\ c^{13}o_{2}^{16} \\ c^{13}o_{2}^{16} \\ c^{13}o_{2}^{16} \\ c^{12}o_{2}^{16}o_{1}^{18} \\ c^{13}o_{2}^{16}o_{1}^{18} \end{array}$	5168.60 5217.63 ^a 5248 ^a 5291.12 5315.696 5349 ^a	$01^{1}2$ $30^{0}1 \leftarrow 02^{0}0$ $02^{0}2 \leftarrow 01^{1}0$ $02^{2}2 \leftarrow 01^{1}0$ $01^{1}2$ $10^{0}2 \leftarrow 01^{1}0$	$\begin{array}{c} c^{13} c^{16} \\ c^{12} c^{16} \end{array}$

^aObserved in present study only; not reported previously.

b Absence of quantum numbers for lower state indicates they are all zero.

^CObserved by Kuiper, 'positions of lines measured later by Diaz. Not observed by Courtoy.

of the spectrum, so that it is not possible to be sure that there is no absorption present. But in view of the fact that our largest sample was considerably bigger than the largest used by Kuiper, and since our spectral resolution is greater than his, it seems likely that the absorption observed by him in this region is due to some gas other than ${\rm CO_2}$ which was present in his sample. Of course, it is conceivable that the abundance of ${\rm O^{18}}$ was greater in his sample than in ours; in which case he would be able to coserve the band when we would not.

Other than for this apparent disagreement near 4505 cm⁻¹, there is good qualitative agreement among the results of the present study and those of Kuiper and Courtoy.

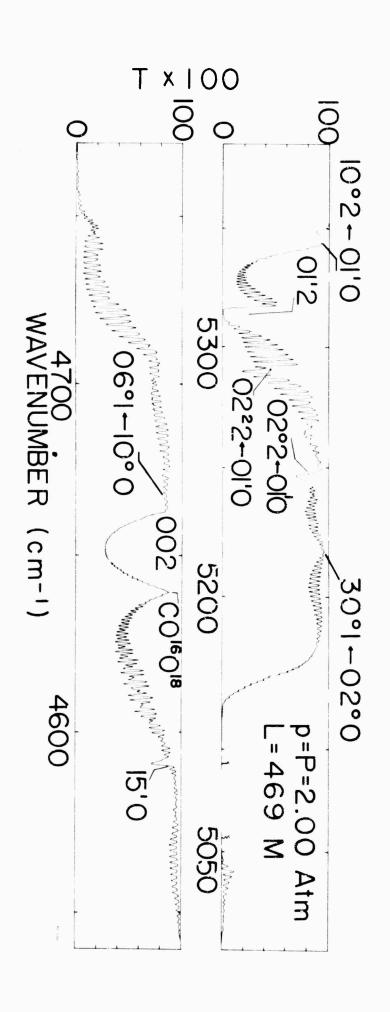
Because of the extremely large samples which were used in the present investigation, five new absorption bands which have not been reported previously were observed. These new bands are included in Table 3-1 and the identifications have been made from our spectra by Dr. William Benedict⁹. A spectrum of a very large sample which shows these new bands is given in Figure 3-1. The two panels of the figure represent the ends of the spectral region considered in this report; the sample is opaque in the regions not shown. The 002 band of CO¹⁶0¹⁸ has been observed by Kuiper⁵ and Diaz⁸, who have measured the positions of several of the lines in this band with very good accuracy. Courtoy has observed the 01¹2 and 02²2+01¹0 bands, but the other bands which are identified in the figure have not been reported previously.

3.2 BAND STRENGTHS

The strength, or intensity of an absorption band is given by $\int K(v)dv$, where K(v) is the absorption coefficient defined by

$$T'(v) = \exp(-K(v)u).$$

 $T'(\nu)$ is the true transmittance at ν which would be observed by a spectrometer with infinite resolution. The strength of a band is proportional to the transition probability and, by the use of theoretical considerations, one can calculate from it the strengths of individual lines within the band. The reverse is, of course, also true; the strength of a band, or at least the strength of one branch, can usually be calculated from the strength of one line.



R07104 FIGURE 3-1. SPECTRUM OF A VERY LARGE SAMPLE OF CO₂ BETWEEN 4540 AND 5380 cm⁻¹

other bands which are identified have not been reported previously. Only a few of the lines 5050 to 5160 cm⁻¹. The broken portions of the curve represent regions where attempts have been made to correct for considerable absorption by $\rm H_2O$. The 002 band of $\rm CC^{16}0^{18}$ has been observed by Kuiper and by Diaz; and Courtoy has observed the 01¹2 and 02 2 +01¹0 bands. The near P20 of the 060 ± 10^{00} band can be observed in the region indicated; the other lines of this band are overlapped by stronger lines. The sample is opague in the spectral regions from approximately 4775 to 5020 cm⁻¹ and from The strengths of many of the bands in this spectral region could be determined from the data presented in this report. However, at the present time, the only bands whose strengths have been considered are the three major ones, $2\nu_1 + \nu_3$, $\nu_1 + 2\nu_2 + \nu_3$ and $4\nu_2 + \nu_3$ and the five new bands which have not been reported previously. The strengths of as many of the branches of these bands as it has been possible to determine are given in Table 3-2.

TABLE 3-2
BAND STRENGTHS

		$\int K(v)dv (atm^{-1} cm^{-1} cm^{-1})STP$				
Transition	v o cm ⁻¹	P	Q	R	Total Band ^b	Total Band Weber et al
	,	. <u>M</u> a	jor Ban	ds		
0401	4853.578	0.11	0.00	0.12	0.23	0.30
1201	4977.793	0.52	0.00	0.53	1.05	1.11
20 ⁰ 1	5099.619	0.15	0.00	0.18	0.33	0.47
		Ne	ew Band	<u>s</u> d		
15 ¹ 0	4591.0	0.16	J.04	0.22	0.42	
$06^{0}1 - 10^{0}0$	4687.75	0.06				
$30^{0}1-02^{2}0$	5217.63		0.00	0.27		
02 ⁰ 2-01 ¹ 0	5248	0.09	0.17	0.07	0.33	
10.02+01 ¹ 0	5349	0.03	0.08	0.03	0.14	

fall bands listed in this Table pertain to the $C^{12}O_2^{16}$ molecule,

The uncertainty in the values for the major bands is about six or eight percent, but it is considerably higher for the new bands.

CValues are taken from Weber, Holm and Penner and multiplied by 300/273 to adjust to density at STP. The authors given an uncertainty of - 20%.

The strengths of the new bands were determined from our raw spectra by Benedict9.

The values given for the new bands should be considered tentative since they were obtained from the "raw" spectra. With some effort it is possible that more accurate values could be determined from the digitized output based on these spectra. Considerably better values could probably be obtained for the new bands from spectra with better resolution for samples containing less $\rm H_2O$ as an impurity.

The strengths of the major lands were determined from spectra of samples at a total pressure of approximately 10 atm. At pressures this high, the lines are wider than the spectral slit width so that the observed spectrum is not greatly different from what would be observed with infinite resolution; i.e., the observed transmittance $T(\nu)$ would be approximately the same as $T'(\nu) = \exp(-K(\nu)u)$. The band strengths were then determined from

$$\int K(v)dv = \frac{1}{v} \int -\ln T(v)dv \tag{4}$$

Strengths of other bands in this region, and possibly some revised values for those listed in Table 3-2, will appear in subsequent reports.

SAMPLE PARAMETERS

The parameters for the 38 samples used in this investigation are summarized in Table 4-1. The path length L and the following pressures are expressed in both atmospheres and torr (mm Hg):

- p partial pressure of CO₂.
- P total pressure due to CO_2 and N_2 .
- Pe the equivalent pressure which accounts for the difference between self-broadening and foreign broadening by nitrogen. It is given by P = 1.3 W p + (P p) where W is a Van der Waals correction given by equation (2).

Reproductions of the spectra of all the samples are shown in Section 5; the page numbers in which the different portions of each spectrum appear are listed in the last six columns of Table 4-1.

The resolution schedule corresponds to the spectral slitwidth of the spectrometer used to record the spectrum. Each schedule is related to slitwidth according to Table 2-1. Spectra of a few samples were obtained with two different resolution schedules; in these cases the same letter was used to identify the sample, but a star was used to denote the different resolution.

The maximum pressure used in the long absorption cell was 2.5 atm; spectra were obtained for the maximum pressure of pure ${\rm CO}_2$ at 4, 8, 16 and 32 passes of the cell. The other samples were chosen so as to provide groups having approximately the same value of absorber thickness, which is given by

$$u = W p L \frac{273}{296}$$
 (1)

TABLE 4-1
SAMPLE PARAMETERS

Sam.	p	P	Pe	P	P	P _e
No.			<u>-</u> -			_
İ						
	torr	torr	torr	atm	atm	atm
a	1900	1900	2500	2.50	2.50	3.29
b	1920	1920	2520	2.53	2.53	3.32
C	1920	1920	2520	2.53	2.53	3.32
d	1900	1900	2500	2.50	2.50	3.29
e	1522	1522	1995	2.00	2.00	2.62
f	760	760	992	1.000	1.000	1.31
g	760	760	992	1.000	1.000	1.31
g*	760	760	992	1.000	1.000	1.31
h	88	88	114	0.116	0.116	0.150
¦ i	175	175	228	0.230	0.230	0.300
i*	175	175	228	0.230	0.230	0.300
j	175	707	759	0.230	0.930	0.999
k	29.4	29.4	38.2	0.0387	0.0387	0.0503
1	58.5	58.5	76.1	0.0770	0.0770	0.1001
1*	58.5	58.5	76.1	0.0770	0.0770	0.1001
m	58.5	212	230	0.0770	0.279	0.303
n	58.5	743	761	0.9770	0.978	1.001
0	8.95	8.95	11.8	0.0118	0.0118	0.0155
P	17.8	17.8	23.1	0.0234	0.0234	0.0304
P	17.8	72	77.3	0.0234	0.0948	0.102
r	17.8	223	228	0.0234	0.293	0.300
۶	507	507	661	0.667	0.667	0.870
t	5.8	5.8	7.54	0.00763	0.00763	0.00992
u	5.8	21	22.7	0.00763	0.0276	0.0299
V	165	165	214	0.217	0.217	0.282
w	165	710	760	0.217	0.934	1.000
x	165	2280	2330	0.217	3.00	3.07
у	49.8	49.8	64.7	0.0655	0.0655	0.0851
z	49.8	213	228	0.0655	0.280	0.300
aa	49.8	776	791	0.0655	1.02	1.04
ab	49.8	2280	2295	0.0655	3.00	3.02
аc	49.8	7600	7615	0.0655	10.00	10.02
ad	49.8	213	228	0.0655	0.280	0.300
ae	49.8	2280	2295	0.0655	30.0	3.02
af	25	7600	7610	0.0329	10.00	10.01
ag	100	7600	7630	0.132	10.00	10.04
ah	3.13	25	25.9	0.00412	0.0329	0.0341
aí	3.13	225	226	0.00412	0.296	0.297
aj	3.13	760	761	0.00412	1.000	1.001
ak	3.13	2280	2280	0.00412	3.00	3.00
al	3.13	76 00	7600	0.00412	10.00	10.00

Sam.	L	Li	Res.	P	ages on	which s	pectra	appear	
	Path	atm cm	Sch.	5375-	5185-	5030-	4905-	4795-	4665-
		STP		518 5	5030	4905	4795	4665	ز 5د45 ز
			ŧ	- l	-1	- 1	-1	-1	-1
	m	017 000	В	<u>cm</u> 5-2	5-4	cm	cm	cm	cm 5 20
a b	933 469	217,000 111,000	В	5-2	5-4			5-16 5-16	5-20 5-20
c	237	55,700	В	5 - 2	5-4	5-8		5-16	5-20
d	121	28,100	В	5-3	5- 5	5-9		5-17	5-21
e	469	87,100	В	5-3	5-5			5 -1 7	5-21
f	933		В	5-3	5 - 5	5-9			5-21
	237	86,200	В	5 - 2	5-4	5-8	5 - 1 2	5 -1 7	5-20
g g*	237	21,900		5 - 3	J-4	5-0	5-12	5-16	•
g^ h	933	21,900	A C	5 - 3	5-5	5-9	5-13	5-17 5-17	5-21 5-21
i	469	9,940	В	5-2	5-4	5-8			5-20
i*	469	9,950 9,950	A	J- Z	J- 4	<i>y</i> 0	5 - 12	5-16 5-18	J-20 j
j j	469	9,950	В	5-2	5-4	5-8	5-12	5-16 5-16	5-20
k	933	•	C	5-2	5-4	5-8			
1	469	3,320		5-2	5-4	5-8	5-12	5-16 5-16	5-20
1*	469	3,320	В	5-2	5-6	5-10	5-12		5-20
	469	3,320	A	5-3	5-5	5-9	5-14	5-18	5-21
m	469	3,320	В	5-3	5-5	5 - 9	5-13	5 - 17	5-21 5-21
n		3,320	В	J- J			5-13	5-17	3-21
0	933	1,010	С		5-4	5-8	5-12	5-16	
р	469	1,010	В		5-7	5-11	5-15	5-19	
P	469	1,010	В		5-7	5-11	5-15	5 - 19	
r	469	1,010	В		5-7	5-11	5-15	5-19	
S	16.5	1,010	В		5-6	5-10	5-14	5-18	
t	469	329	В		5-6	5-10	5-14	5-18	
u	469	329	В		5-4	5-8	5-12	5-16	
- v	16.5	330	В		5-5	5-9	5-13	5-17	
w	16.5	330	В		5-5	5-9	5-13	5-17	
x	16.5	330	В		5-4	5 - 8	5-12	5-16	
у	16.5	99.6	В		5 - 7	5 - 11	5-15	5-19	
•-	16.5	99.6	В		5-6	5-10	5-14	5-18	
aa	16.5	99.6	В		5-4	5-8	5-12	5-16	
ab	16.5	99.6	В		5-6	5-10	5 - 14	5-18	
a c	16.5	99.6	В		5 - 5	5-9	5-13		
ad	4.16	25	В		5-6	5-10	5-14		
ae	4.16		В		5 - 5	5-9	5-13		
af	8.26		В		5 - 5	5-9	5-13		
ag	4.16	50.3	В		5 - 5	5-9	5-13		
ah	16.5	6.26	В			5-11			
ai	16.5	6.26	В			5-9			
аj	16.5	6.26	В			5-9			
ak	16.5	6.26	В			5-9			
al	16.5	6,26	В		ir	5-8			

TRANSMISSION SPECTRA

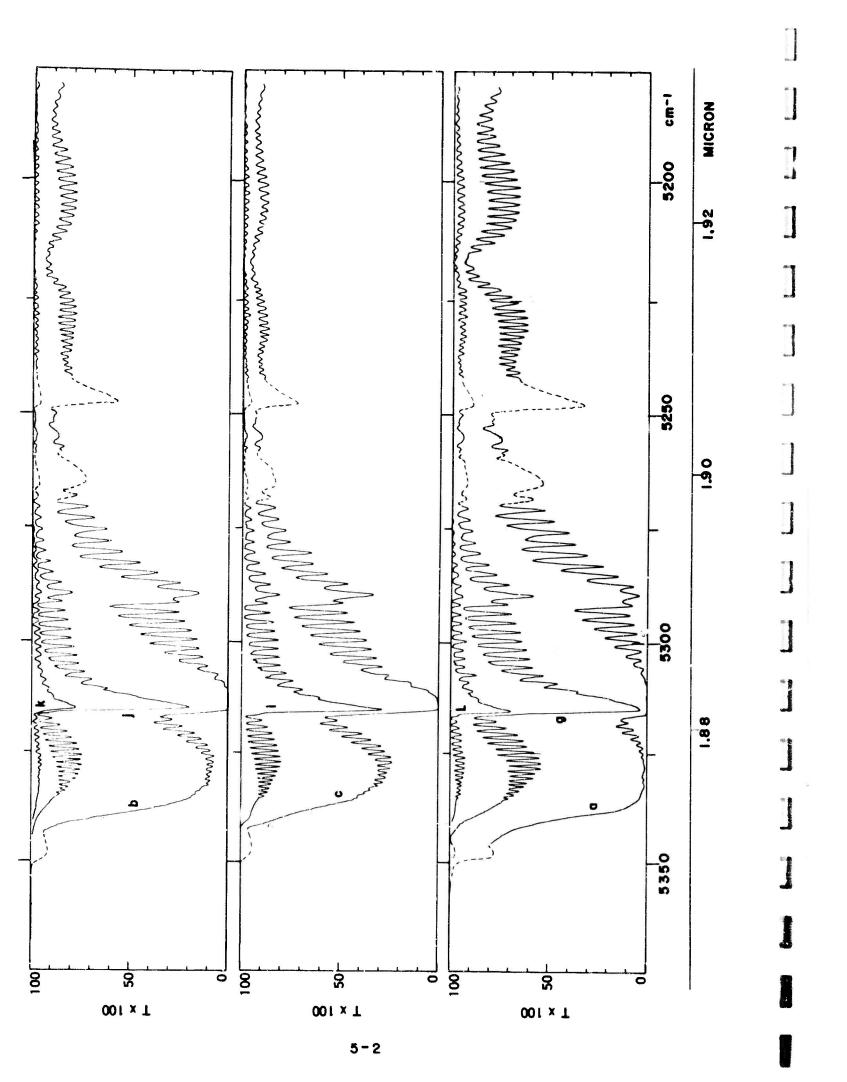
Reproductions of the spectra of 38 samples are shown in this section. The spectra were traced from the originals by use of the equipment described in Appendix C. The spectra are so long that they were divided into the following six regions:

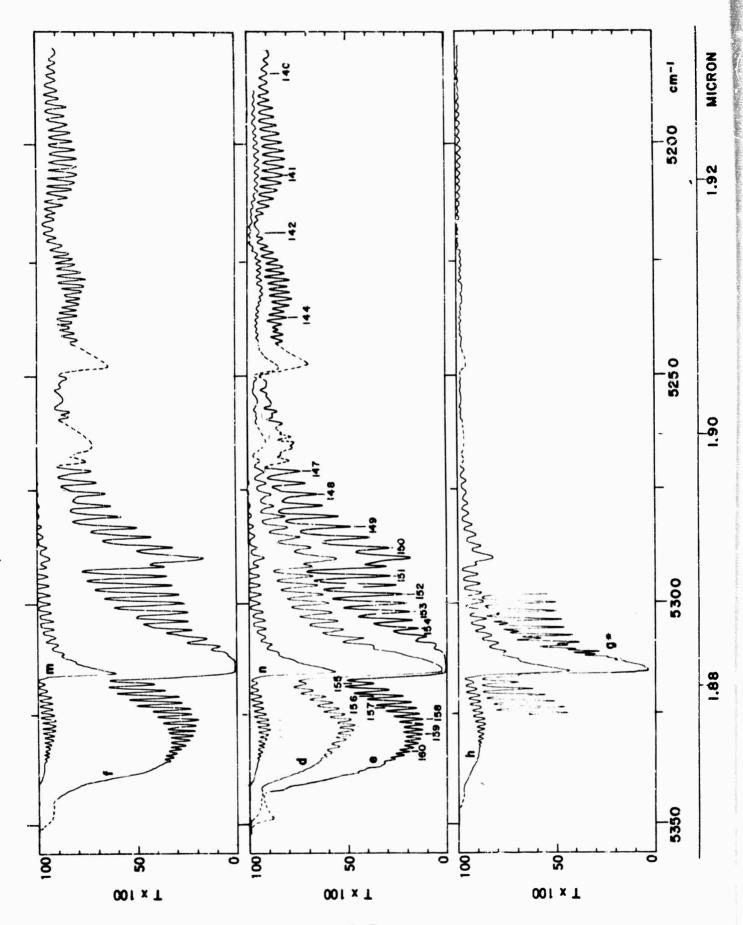
Sp_ctral Region	Pages
5375 - 5185 cm ⁻¹	5-2, 5-3
5185 - 5030	5-4 to 5-7
5030 - 4905	5-8 to 5-11
4905 - 4795	5-12 to 5-15
4795 - 4665	5-16 to 5-19
4665 - 4535	5-20, 5-21

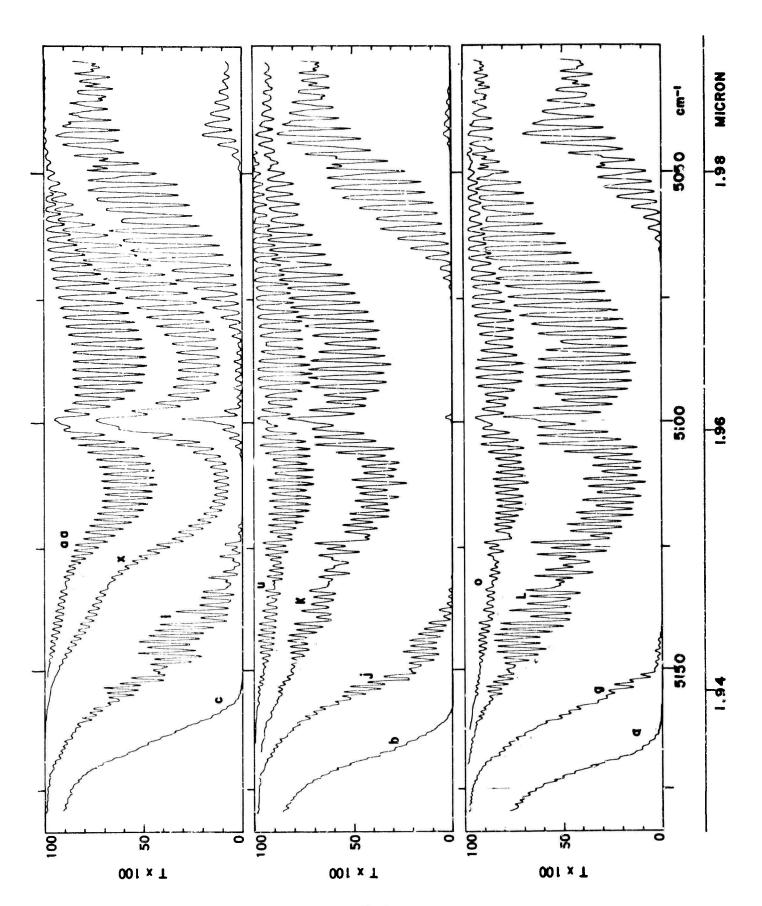
The wavenumber scale is accurate to approximately - 1 cm - 1; more accurate values of line positions can be obtained from Courtoy or by interpolating between the designated calibration points. In some cases the original spectra of samples represented in the same panel in a figure were obtained at quite different times when the wavenumber calibration of the spectrometer was different, and the retraced spectra do not always "nest" properly. There is a slight periodic error in the screw which rotates the grating; therefore, the calibration shift was not linear in wavenumber. Calibration points were taken sufficiently close together that it can be assumed the spectra are linear between them; but the periodic error in the screw would in some cases cause significant error in calibration if one were to assume a spectrum was linear over an interval as wide as 20 or 30 cm - 1. The positions of known H₂O and CO₂ lines used for calibration are indicated by numbers in the figures, and the corresponding wavenumbers are listed in Table 5-1.

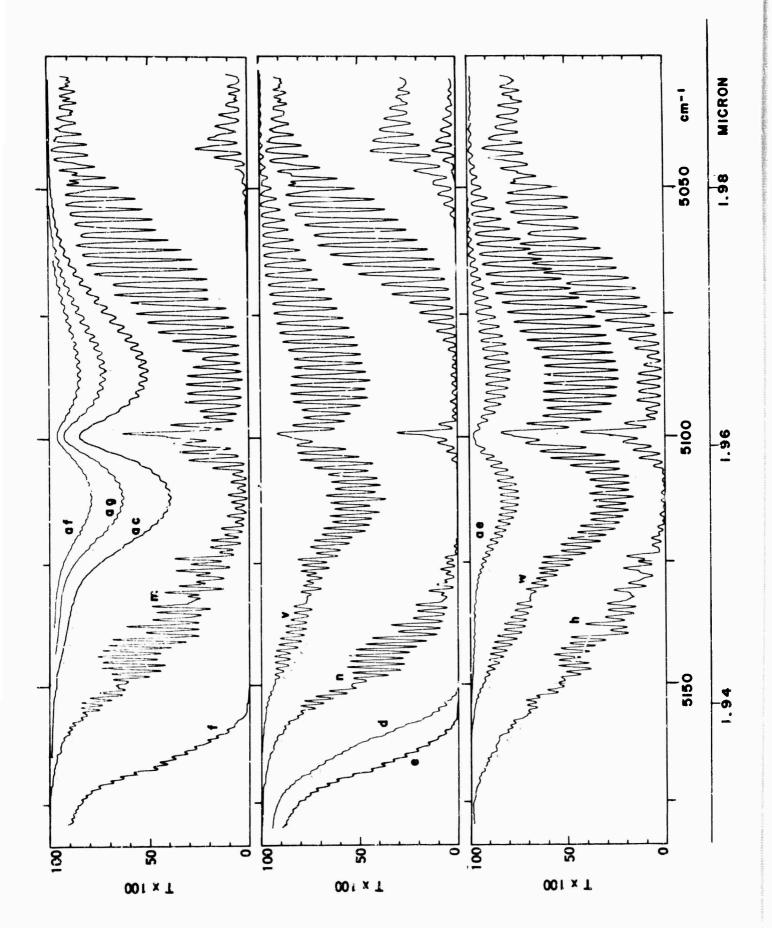
Each sample is designated by the same letter as that given in Table 4-1. The spectra designated by starred letters correspond to the same sample as the unstarred letter, but the spectrum was obtained with higher resolution in order to resolve more lines and to determine more accurate positions of the line centers. No calculations of transmittance or integrated absorptance were made from the spectra marked with stars.

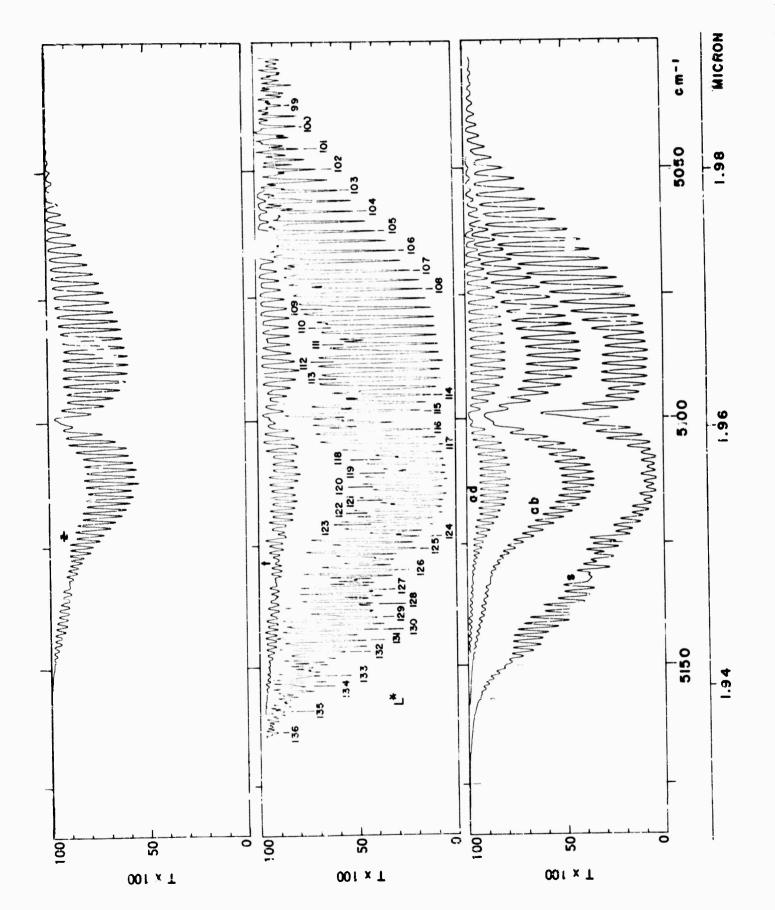
Regions where the ${\rm CO}_2$ absorption was difficult to observe because of overlapping absorption by ${\rm H}_2{\rm O}$ are indicated by dotted lines. Portions of some spectra were omitted where the absorption was small, particularly when spectra of larger samples having greater absorption in the same region are included.

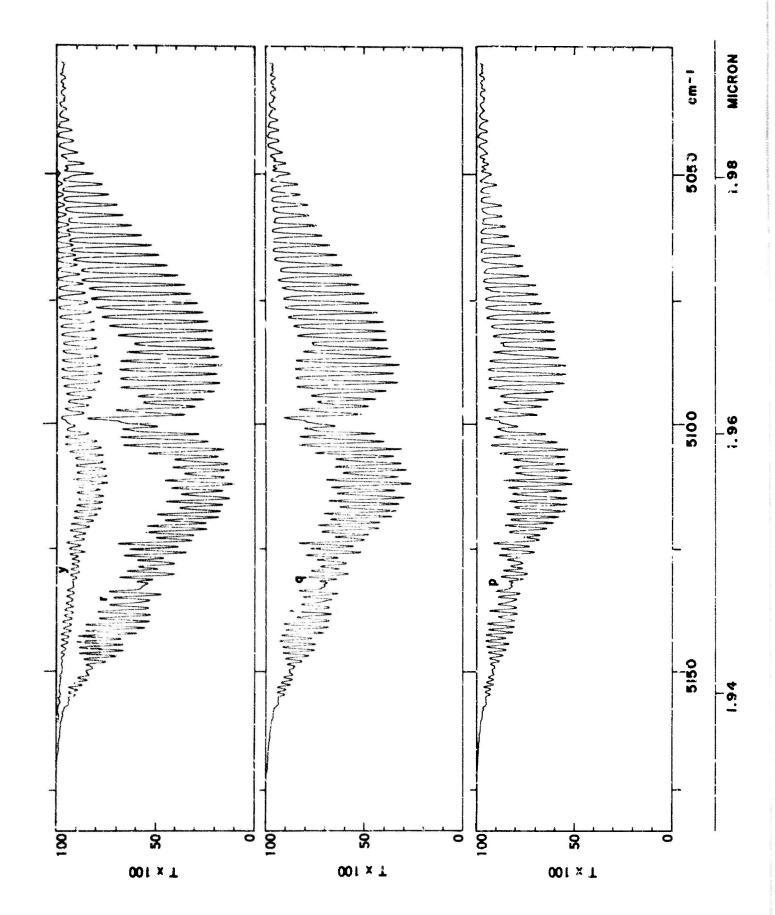


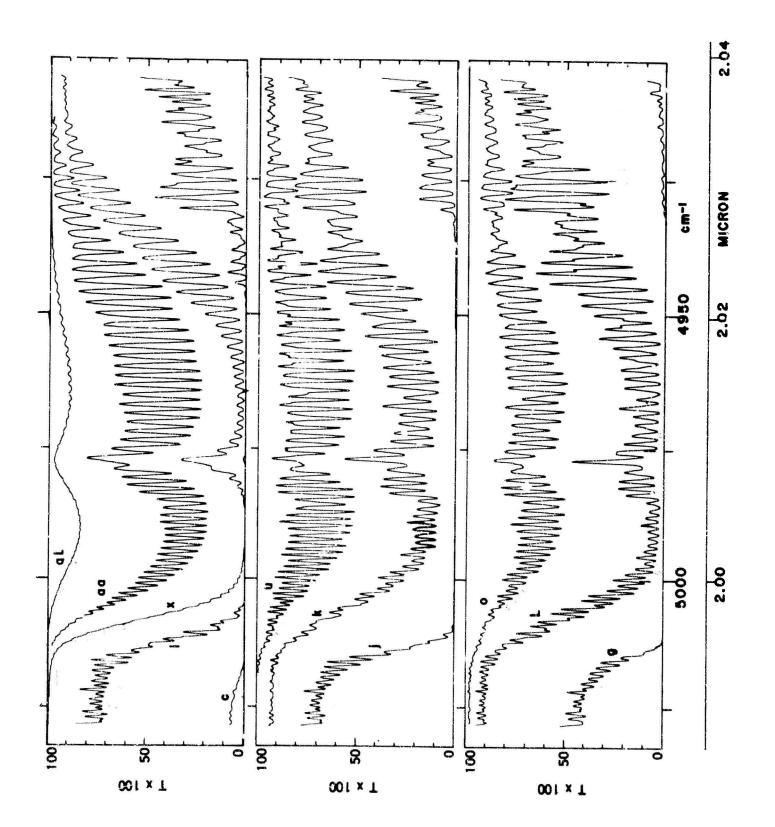


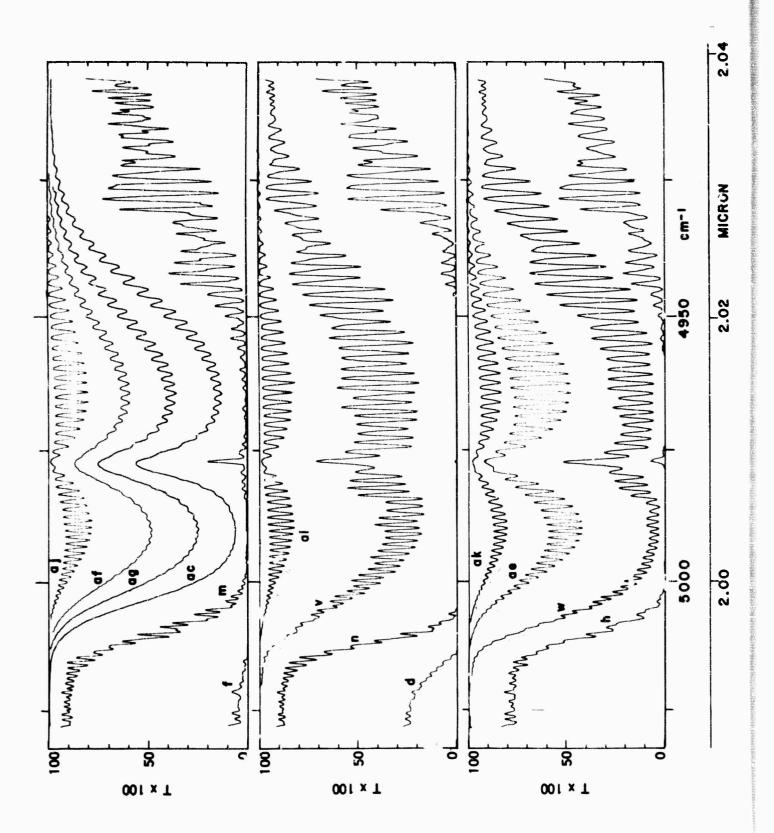


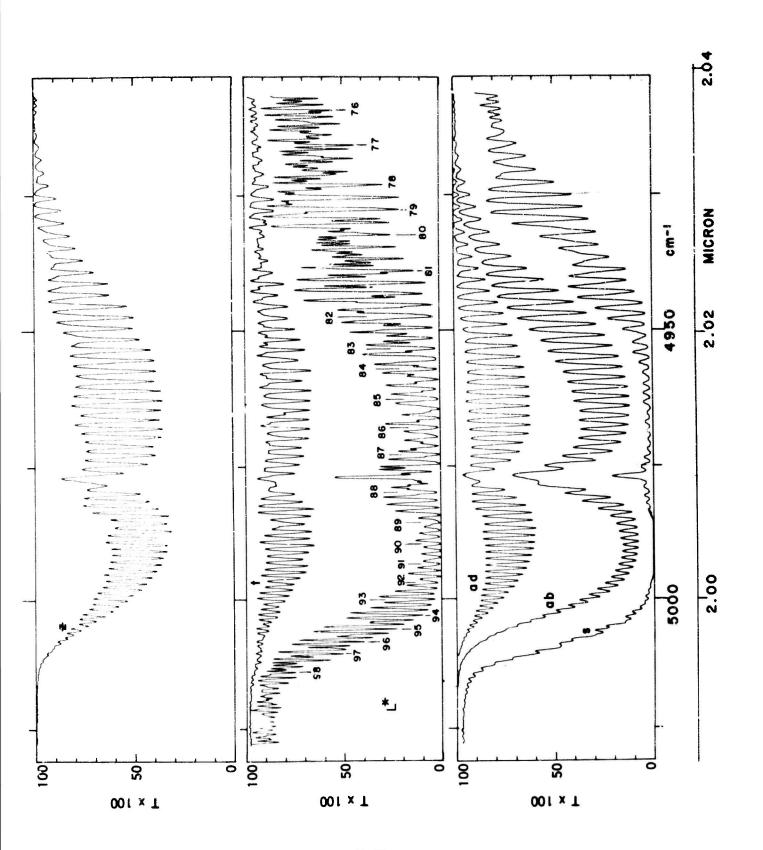


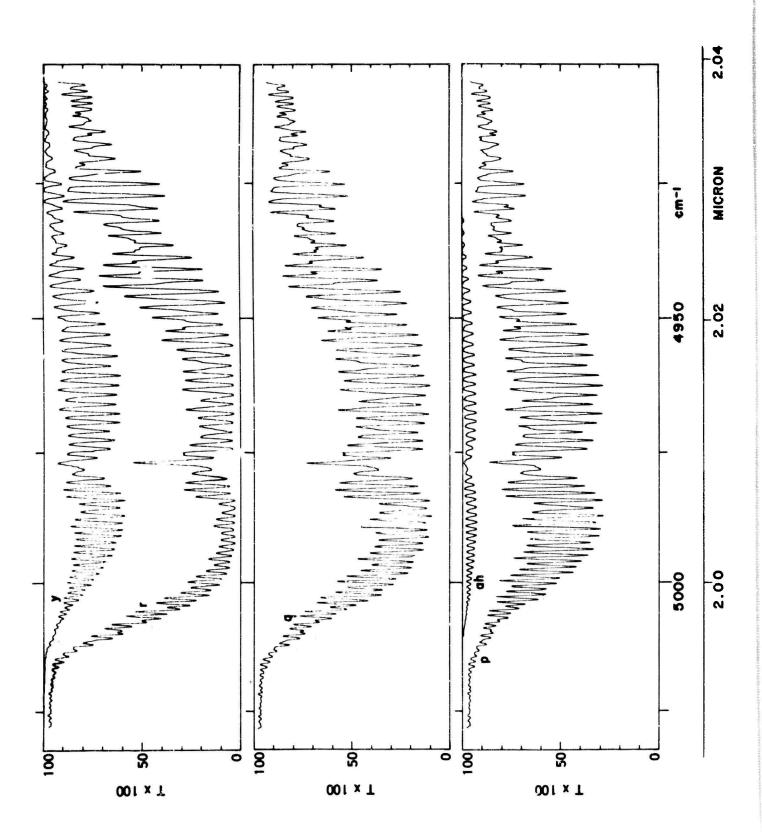


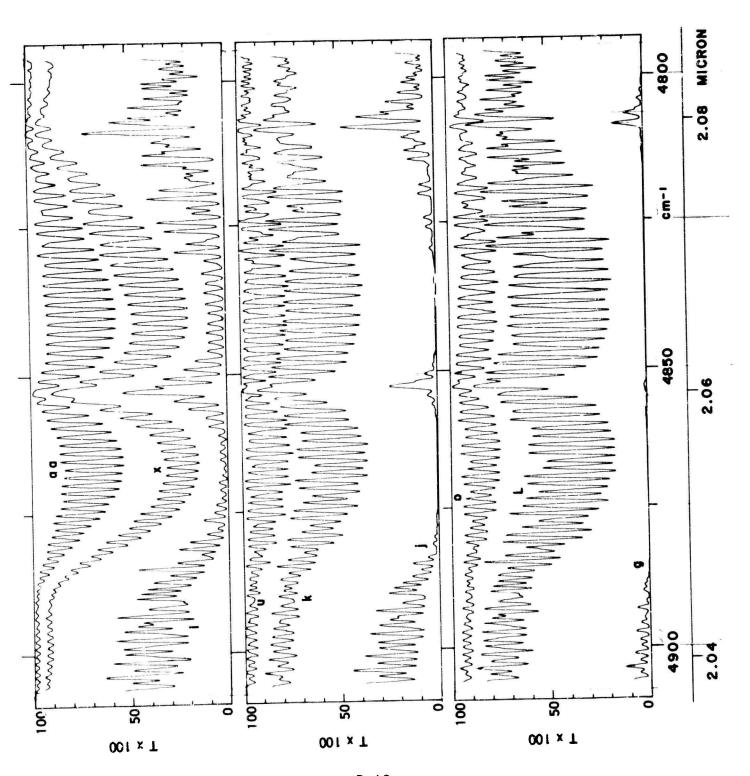




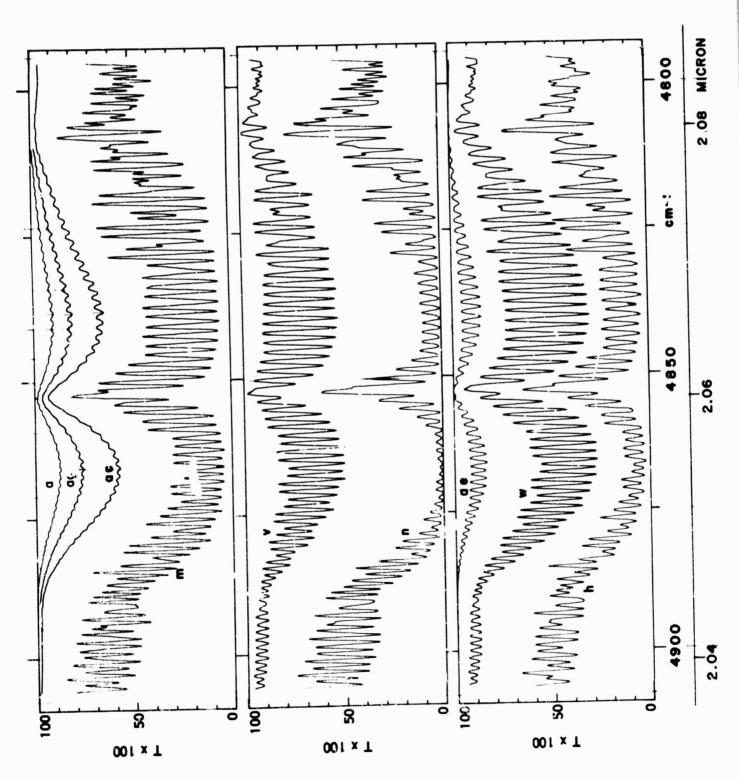


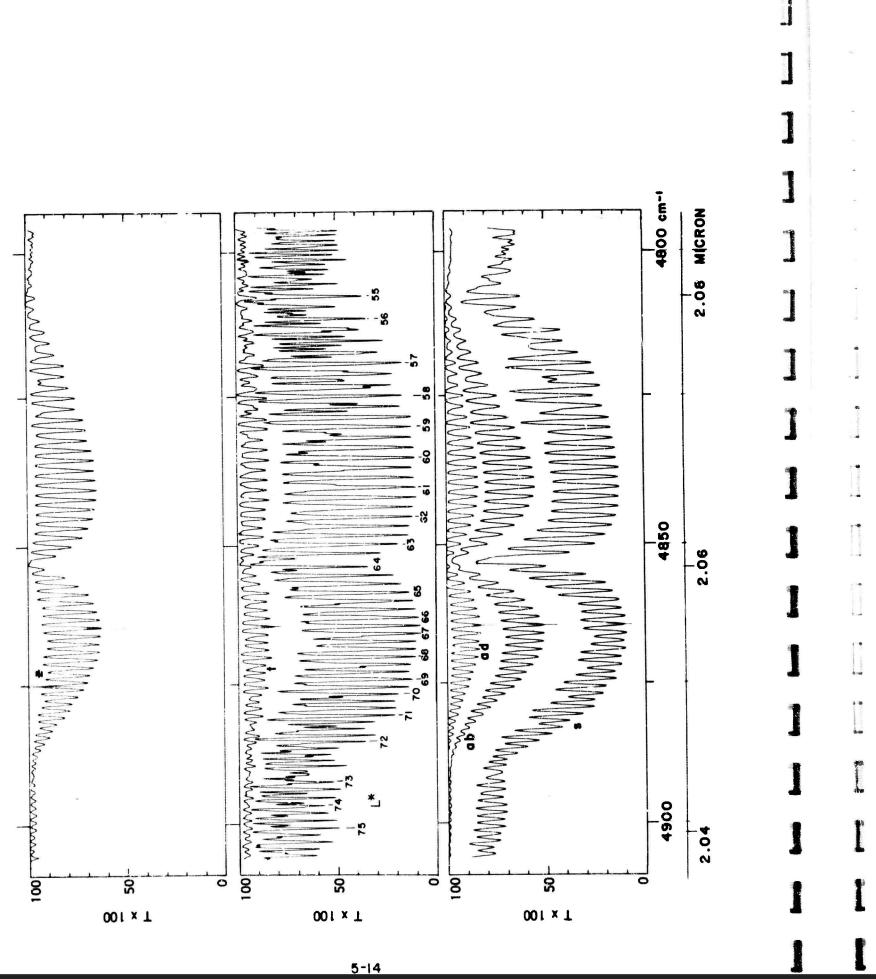


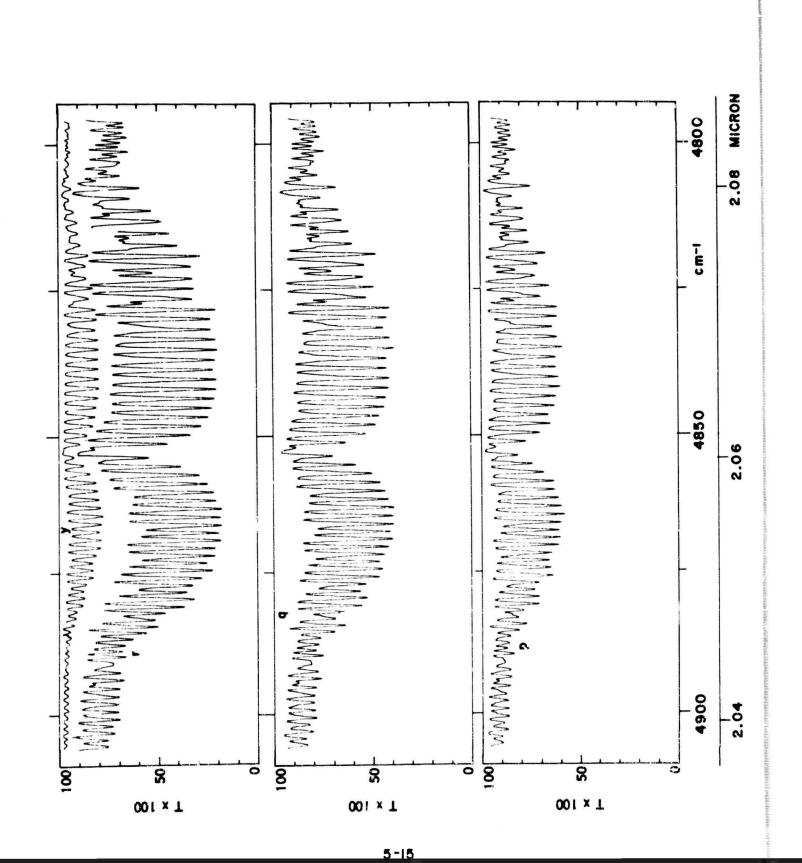


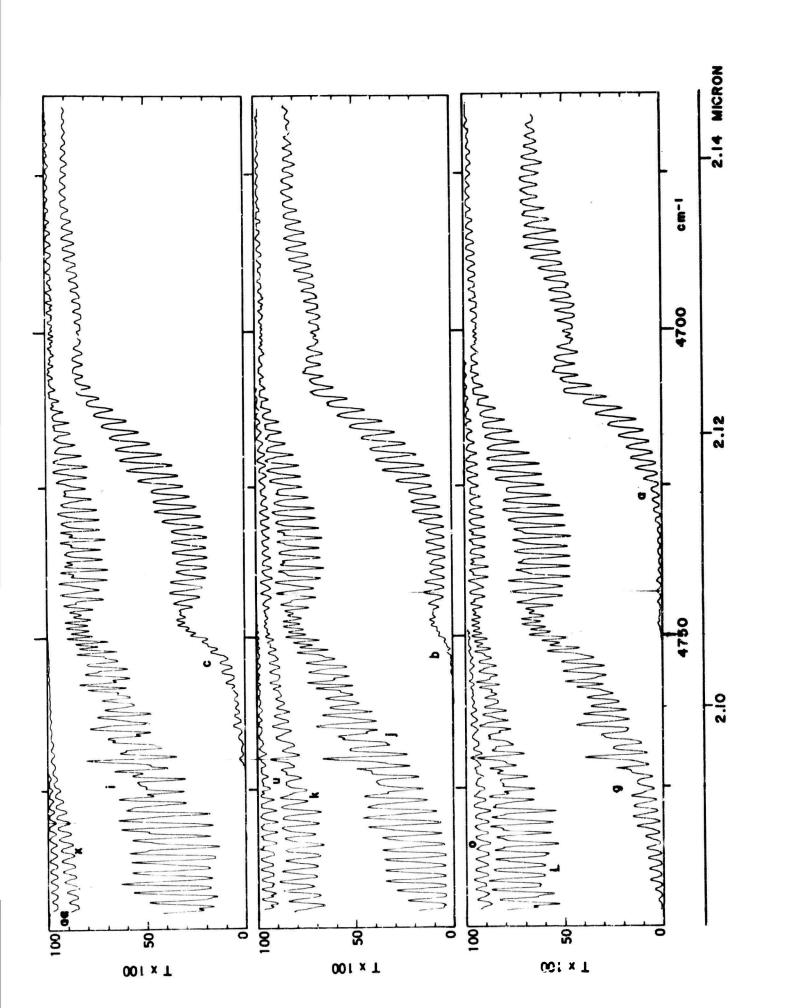


5-12









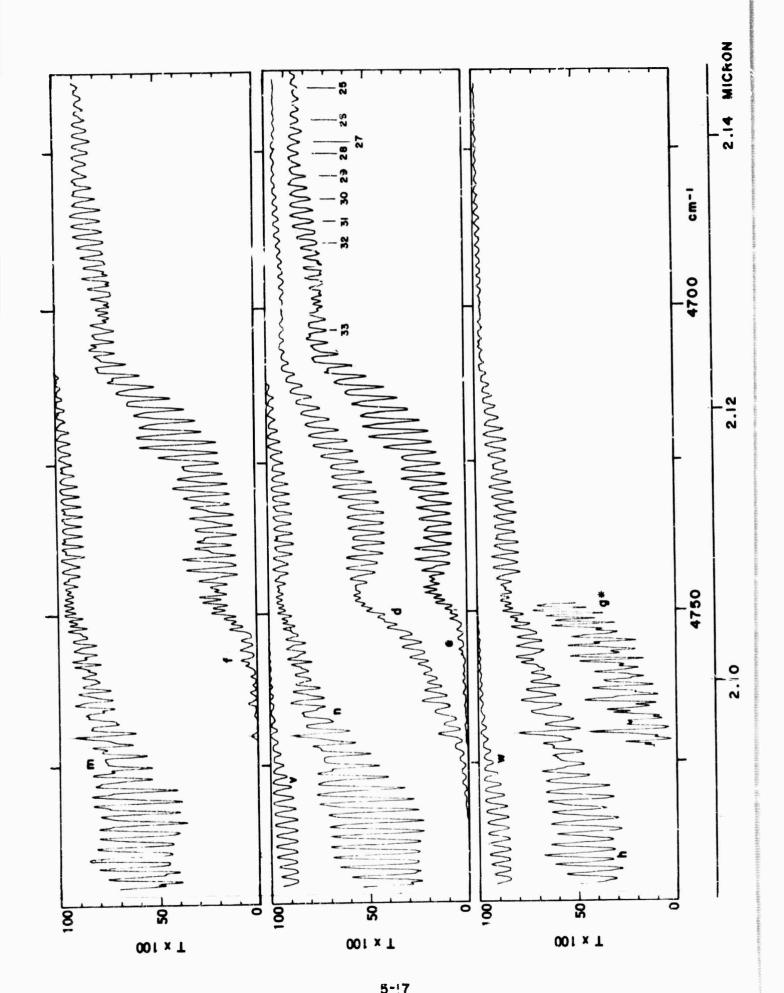
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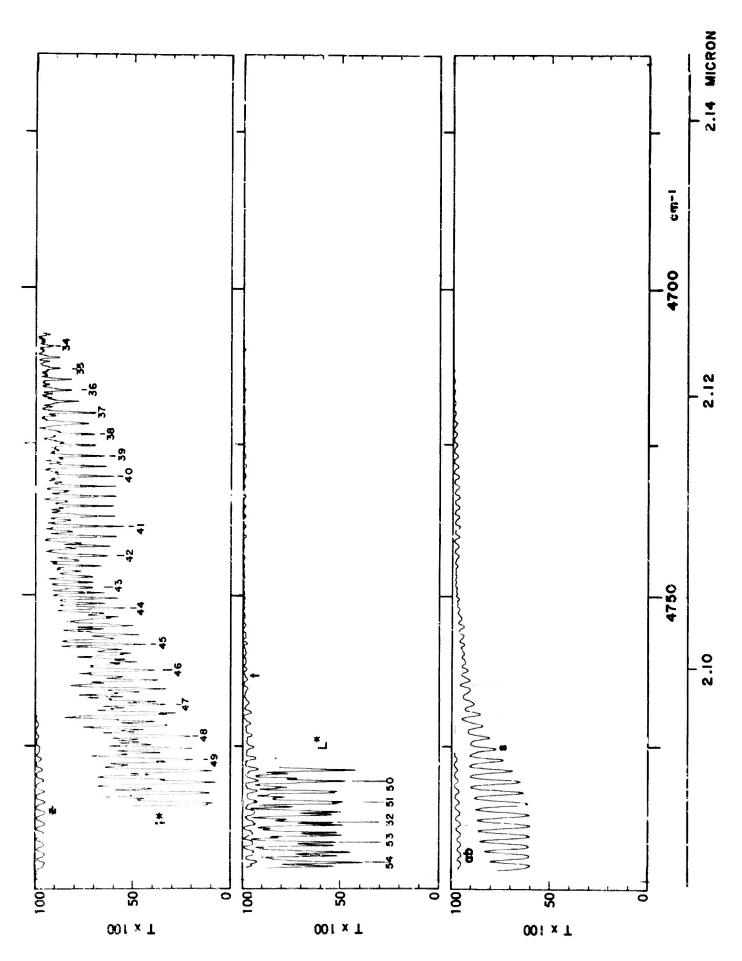
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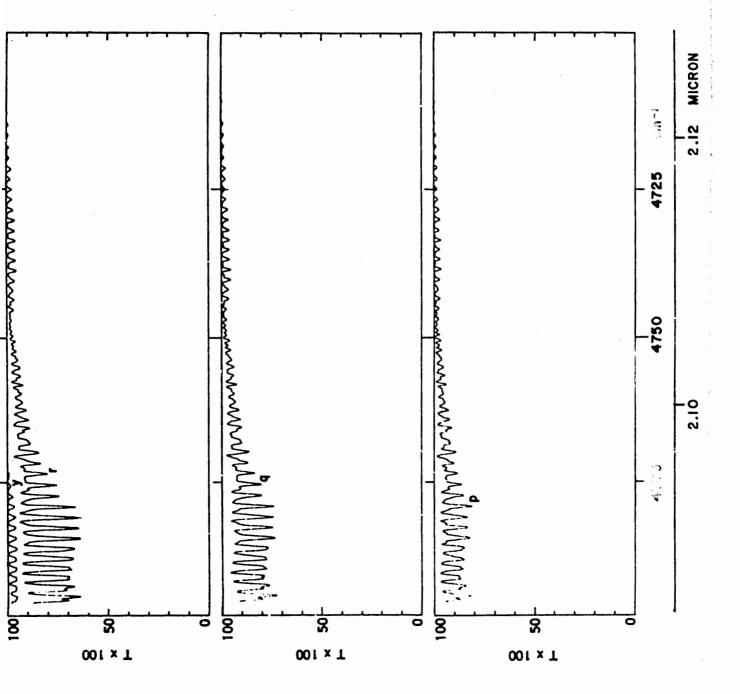
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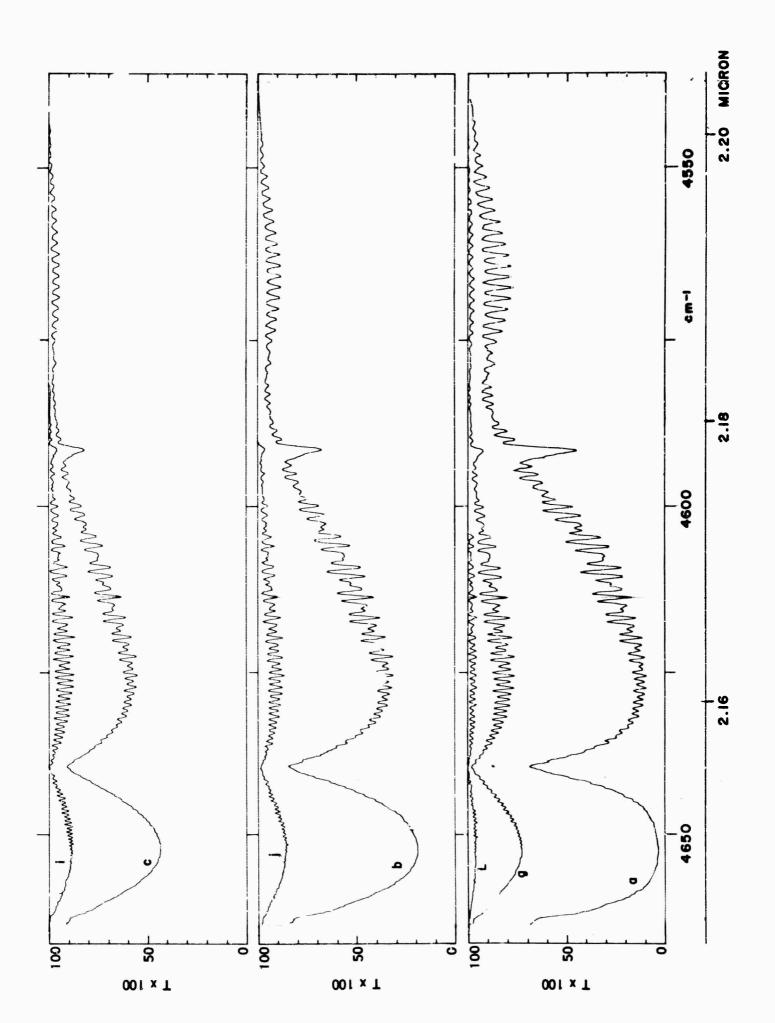
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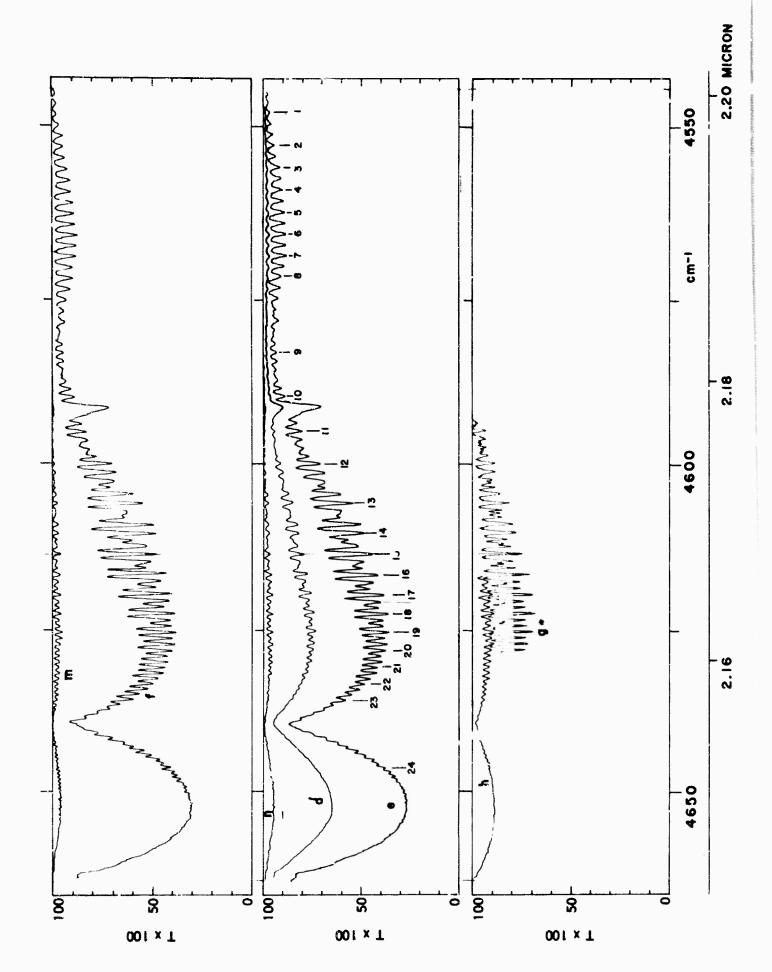


TABLE 5-1
CALIBRATION TABLE

Line No.	ν cm-1	Line V No. cm ⁻¹	Line v No. cm	Line v -1 No. cm	Line v No. cm ⁻¹
1	4548.1	36 4716.3	71 4880.7	106 5066.2	141 5206.6H
2	4553.0	37 4719.9	72 4885.4	107 5070.1	142 5218.4H
3	4556.2	38 4723.4	73 4892.8	108 5073.9	143 5225.3H
4	4559.4	39 4726.8	74 4896.9	109 5077.6	144 5236.9
5	4562.6	40 4730.2	75 4900.9	110 5081.2	145 5254.8H
6	4565.8	41 4738.5	76 4909.1	111 5084.8	146 5264.1H
7	4569.0	42 4743.3	77 4915.1	112 5088.2	147 5270.7
8	4572.1	43 4748.8	78 4922.8	113 5091.6	148 5275.7
9	4583.2	44 4751.8	79 4927.5	114 5094.9	149 5282.8
10	4589.6	45 4757.9	80 4932.1	115 5098.1	150 5287.4
11	4594.7	46 4762.3	81 4938.7	116 5101.9	151 5293.8
12	4599.7	47 4767.8	82 4947.1	117 5104.9	152 5297.9
13	4605.6	48 4773.3	83 4953.2	118 5107.8	153 5301.9
14	4610.1	49 4777.2	84 4957.0	119 5110.7	154 5305.6
15	4613.4	50 4780.9	85 4962.6	120 5113.4	155 5318.0
16	4616.6	51 4784.4	86 4967.9	121 5116.1	156 5320.8
17	4619.6	52 4787.9	87 4973.0	122 5118.6	157 5323.5
18	4622.6	53 4791.4	88 4980.1	123 5121.1	158 5326.0
19	4625.4	54 4794.7	89 4985.9	124 5123.5	159 5329.5
20	4628.1	55 4807.4	90 4989.9	125 5125.9	160 5333.4
21	4630.8	56 4811.4	91 4993.7	126 5130.3	161 5344.9Н
22	4633.3	57 4819.1	92 4997.2	127 5134.5	162 5348.7н
23	4635.7	58 4824.7	93 5000.4	128 5137.2	163 5364.2Н
24	4646.3	59 4830.2	94 5003.4	129 5139.8	164 5377.0H
25	4666.6	60 4835.5	95 5006.1	130 5142.4	
26	4671.6	61 4840.6	96 5008.5	131 5144.8	
27	4675.1	62 4845.6	97 5010.7	1.32 5147.1	
28	4676.9	63 4850.4	98 5014.2	133 5151.9	
29	4690.6	64 4854.4	99 5037.3	134 5154.1	
30	4684.1	65 4858.9	100 5041.6	135 5159.4	
1				1	
31	4687.6	66 4863.3	101 5045.9	136 5163.7H	
32	4691.0	67 4866.2	102 5050.1	137 5170.5H	
33	4705.3	68 4870.4	103 5054.2	138 5176.2H	
34	4709.1	69 4874.4	104 5058.3	139 5180.6H	
35	4712.7	70 4877.0	105 5062.3	140 5184.9н	

 $^{^{\}rm H}_{\rm The}$ calibration lines designated with an H are taken from ${\rm H_2O};$ while the remainder are from ${\rm CO_2}.$

SECTION 6

TABLE OF TRANSMITTANCES

Table 6-1 consists of values of transmittance, in percent, recorded at intervals of 0.1 cm⁻¹ in the region from 4536 to 5362 cm⁻¹. The interval is sufficiently small that the original spectrum could be approximated very closely by plotting the tabulated values and joining the points with straight lines. The first column gives the wavenumber in cm⁻¹, and the second column gives the corresponding wavelength in microns. The tables were made by photographing a portion of the computer output which was obtained from the spectra by the technique described in Appendix C.

The ${\rm CO}_2$ partial pressure p, the equivalent pressure ${\rm P}_{\rm e}$ and the absorber thickness u for each sample are shown at the top of the column corresponding to that sample. These sample parameters are repeated on alternate pages for convenience. Each sample is designated by the same letter as in Table 4-1 and in the spectra in Section 5.

Values of transmittance are not tabulated over the entire spectral region for several of the smaller samples since the absorptance in some portions is very small. All tabulated values for a given wavenumber appear on a single page. Several of the larger sample are opaque over rather wide spectral intervals; in such cases a note stating that T=0 is included rather than repeating all the hundreds of zero's which would otherwise appear.

The wavenumbers of most of the line centers are accurace to $\stackrel{+}{-}$ 0.1 cm $^{-1}$ in the tables. Only a few are in error by more than 0.2 cm $^{-1}$.

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| # 10°2<br>10°2<br>10°4<br>10°4<br>10°4<br>10°4             | 8                                                     | *****                                                       | 17772                                   | *****                                   |                                                     | 7 0 0 7 7 7                                | 17717                                                       |                                        | *****                                                   |                                         | *****                                       |                | *****                                   | ?????  | :::::       |                                       |                  | 10000                                   |   |
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| * ** ** * * * * * * * * * * * * * * *                      | 957555                                                |                                                             |                                         |                                         |                                                     |                                            |                                                             |                                        |                                                         |                                         |                                             |                |                                         |        |             |                                       |                  |                                         |   |
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|                                                            | 9 4 1418                                              |                                                             |                                         |                                         |                                                     |                                            |                                                             |                                        |                                                         |                                         |                                             |                |                                         |        |             |                                       |                  |                                         |   |
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| Hamma, Man,<br>principal)<br>(action complication)         |                                                       | ***                                                         |                                         |                                         |                                                     |                                            |                                                             |                                        |                                                         |                                         |                                             |                |                                         |        |             |                                       |                  |                                         | - |
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PRESENT MARKE CHANNE BENDE BERTT ARBEN KONGE EPRTT PER ET ARRE COURT COURT COURT ARRES CHANNE ABRES CHANNE PROPER BETTA COURT A MANDO THAT THAT THE BOOK AND APPEN PROPERTURE STORE SAME SAME THAT STORE THE TOTAL THE SAME AND A MANDA AND THE THAT A THAT I SAME AND THAT THE SAME THAT THE SAME AND THAT THE SAME THAT PORPY TOTUS AGENT NESS STATE STATE THE ARREST AGENT TOTAL TOTAL TOTAL STATE STATE SALE THE SALE SALE THE STATE TOTAL TOTAL TOTAL TOTAL TOTAL TOTAL THE SALE TE HER MYTHE CHARL THE TOTAL THE PROPERTY SERVED THE THE PROPERTY OF THE PROPE THE STATE ST PORT | MOPER MORRIS BATAN BROWN FOUR ANDRES PRINCE PRINCE STREET FARRA GARAF PRINCE FRRIE MARRE ACT ACADA WARRE BROWN BROWN ALL STREET ACADA WARRE WAR - ኮቴሽሲ ኮቴሽሲያ የተመመ የመመመ መመመው መመመው መመመው የተመታዩ የሚመታው መለመው መስመው ለስፋቆጠ ቀመሰው መመሰለዊ መመሰለዊ መመስለ መለቀል ለመለፈት ለተለከ ለሚቀው ተመጠለር 1 111 - 111 - 111 - 111 - 111 - 111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 11 MATAN BRANC BERNE CTOR AND THE PERSON RASET CAMEN ATTAN PARTY STORE STREET STRE aria typro 1986 film film this tive time from the base from the film to the this film film the film the film the akung tabun 1998. Sibir dalah dalah tahun tabun yang hang balun malah babun batan batan balun sebag bahan mang Burus burus balun bers babun bers burun turus burus burus barus babun bersh bapun balun burus bersh bersh bersh a tala sibba talah antan sala sala sala sala salah Babab babab babah babah salah salah salah salah salah babah babab salah babab salah salah salah baba babah salah THE ROLL STORY STREET STORY STREET ARTH ARREA THAN THAN INTER FORT WHIT INTER SAME AREA THAN INTER TOUR INTER THAN THE TRANSPORT FOR THAN AREA SAME appen datch total tales tales attal tales tales lates total tales total tales tales being about tales being attal being attal tales tales and tales tales attaled to tales and tales attales and tales attales TOTAL TRANSPORT OF THE PROPERTY OF THE PROPERT

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|    | F. 00.1                                 | 2 8 2                  | 8                                       |                                       | *****                                 | *****  | **:      | *****                                       | :::::                                      | ::::::                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | :::::                          | :::::                                                        | :::::                                   | :::::                                     | :::::                                 | 4 4 4 4 4                             | 14414                                     | *****                                               | *****                                                | :::::                                  |
| 1  | * * * * * * * * * * * * * * * * * * *   | <u> </u>               | 8 55555<br>+ + 11111                    | 77111                                 |                                       | :::::  | :::::    | 11111                                       | 11111                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 111111                         | 111111                                                       | *****                                   | :::::                                     | ****                                  | :::::                                 | *****                                     | *****                                               | ****                                                 |                                        |
|    | 11 <u>0</u> 8                           |                        | 27.000                                  |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
|    | 35<br>30-2                              |                        | 0 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
|    | 33. 6                                   |                        | B 4 4 4 4 4                             |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
|    | 10.5                                    | •                      | 819177                                  |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
|    | 20.0                                    |                        | ļ                                       |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                | _                                                            | -                                       |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
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|    | 10.4<br>(19.4                           |                        | 8 1 1 1 1                               |                                       | :::::                                 | :::::  | <i></i>  | :::::                                       |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 11111                          | !!!!!                                                        | }}}}                                    | 17777                                     | *****                                 | 11111                                 | 11711                                     | 11111                                               | 11111                                                | 11911                                  |
| 1  | 1,200                                   | 9 8 9                  | 27.001.1<br>1.11111.1                   | 11111                                 |                                       |        | *****    | *****                                       | 17117                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                | *****                                                        |                                         | *****                                     |                                       | :::::                                 | 11111                                     |                                                     | *****                                                | 11777                                  |
|    | 2,43                                    | 1.00 P                 | E                                       | *****                                 |                                       | 7777   | ::::::   | *****                                       |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | :::::                          | :::::                                                        | * ****                                  | *****                                     | ******                                | 17517                                 | :::::                                     | 11111                                               |                                                      | 11111                                  |
| ١. | 7,e3<br>a 10°3                          | 1 10 x                 |                                         | *****                                 |                                       | :::::  | 22125    | :::::                                       | * ****                                     | :::::                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | , an                           |                                                              | nairi<br>rijri                          | 12222                                     |                                       |                                       | 11111                                     | :::::                                               |                                                      | *****                                  |
|    |                                         | 10,24<br>3,24<br>x 10° | 1:::::                                  | *****                                 |                                       | *****  | *****    | :::::                                       |                                            | 11111                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |                                | 11111                                                        | 7 * * * * * * * * * * * * * * * * * * * |                                           | 111111                                |                                       |                                           |                                                     |                                                      |                                        |
|    | 1.61                                    |                        | \$ + 0 0 0 T                            | ****                                  |                                       | 11111  |          | 11111                                       | 11111                                      | 11117                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 1000                           |                                                              | ****                                    |                                           | ****                                  |                                       |                                           | *****                                               | *****                                                |                                        |
|    | # 10.5<br>10.00                         |                        | 204510                                  |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
|    | # B B                                   |                        | 59999                                   |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
| ١. | . ## <b>8</b>                           | 10°P<br>10³            | 9                                       |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
|    | 1.38                                    | 10.0                   | * 1 7 1 7 1                             |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
|    | TILL SE                                 |                        | g + 55.5.5                              |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
|    | 10°.7<br>10°.7<br>103 1.                | 4 4 4                  | 1                                       |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
|    | 7 7 1.00 PM                             | 4 · •                  | 8                                       |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
|    | r • =                                   | aria:                  | 8                                       |                                       |                                       |        |          |                                             |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
|    | <i>*</i> * *                            | * * * *                | 8 :::::                                 | ****                                  |                                       | 2222   | 27222    | # # # # # # # # # # # # # # # # # # #       |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                |                                                              |                                         | *****                                     | 2005                                  | 11:11                                 | iliti                                     | 22222                                               |                                                      | 2222                                   |
|    | 3 E                                     | • • •                  | 2 - 2222                                |                                       | ****                                  | 1111   |          | 71177                                       |                                            | 5 82 2 7                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |                                | * * * * * * * * * * * * * * * * * * *                        |                                         | *****                                     | 11111                                 | 11111                                 | ::::::                                    | *****                                               |                                                      | ************************************** |
| -  | 01 × 10 × 10 × 10 × 10 × 10 × 10 × 10 × | 7.65                   | 91<br>1                                 |                                       |                                       | ****   | *****    | 7 1111                                      |                                            | :::::                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | *****                          | 7.44.1.<br>7.22.22                                           | *****                                   | *****                                     |                                       | *****                                 |                                           | ****                                                | 11111                                                | :::::                                  |
|    | 1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m | 101 H                  | 8 *****                                 | ****                                  | F-60-6                                | 71777  |          |                                             | :::::                                      | 11111                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 11111                          | * * * * * :<br>E                                             | :::::                                   | *****                                     | 10:11                                 | 11111                                 |                                           | 11111                                               | *****                                                | *****                                  |
|    | 200                                     | × 10, 1                | <u> </u>                                | *****                                 | *****                                 | 10000  | 2222     | ****                                        |                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | :::::                          | 13333                                                        | 11111                                   | 11111                                     | 22333                                 | 11777                                 | 11111                                     | 1222                                                | <br>                                                 | 3333                                   |
|    |                                         |                        |                                         |                                       |                                       |        |          | Ť =                                         | ë Pëk Sari                                 | Matta, e, a                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | $_{2}$ $+$ , $x$ and $\hat{t}$ | IN THIS EPP                                                  | CTRAL REGION                            |                                           |                                       |                                       |                                           |                                                     |                                                      |                                        |
|    |                                         |                        | # # £555E                               | 12212                                 |                                       | 72222  | 12522    | 2 22 2 2                                    | 12553                                      | 22275                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 15315                          | EDEE!                                                        | 1111                                    | IIISE                                     | 2 2 4 - 2                             | 51155                                 | A 45 84                                   | 200027                                              | 0 <b>1</b> 0 5 7                                     | 电电弧电电                                  |
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| ****          |                                       | ***** |                                         | iiiii       |                                       |                                        |                                               |                                                               |                                                  | 22222                                   |                                         |                                                    |                           | *****                                     |                                         |                                         | 12111                                   | ****        | , , , , , ,<br>; ; ; ; ;                | ::::::                                               |
| :::::         | 71111                                 |       | :::::                                   | *****       | :::::                                 | :::::                                  |                                               |                                                               | :::::                                            |                                         | :::::                                   |                                                    |                           | *****                                     | 7 4 4 4 5                               | :::::                                   | *****                                   | :::::       | 7 4 7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | 71155                                                |
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| :::::         | 11111                                 |       |                                         |             |                                       |                                        |                                               | 7::::                                                         |                                                  | :::::                                   | :::::                                   | :::::                                              |                           |                                           | * * * * * * * * * * * * * * * * * * * * | 17777                                   |                                         |             |                                         |                                                      |
| :::::         | 11111                                 | iiiii | fills                                   | :::::       | :::::                                 |                                        |                                               | *****                                                         | :::::                                            | :::::                                   |                                         | * 555.                                             | :::::                     | * 70 9 4<br>* 70 4 4<br>* 70 4 4          |                                         | :::::                                   | :::::                                   | :::::       | :::::                                   | 11111                                                |
| ****          |                                       | ::::: | :::::                                   | :::::       | : : : : : :                           |                                        | :::::                                         | *****                                                         |                                                  | *****                                   |                                         | *****                                              | 11111                     | # # # # # # # # # # # # # # # # # # #     | 17111                                   |                                         | ::::::                                  | :::::       | *****                                   | :::::                                                |
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|               |                                       | ***** | ::::::                                  | *****       |                                       | ****                                   | :::::                                         |                                                               | *****                                            | *****                                   | :::::                                   | *****                                              | *****                     |                                           |                                         | 11111                                   |                                         | *****       | ######################################  | 11111                                                |
| ::::          |                                       |       | 12715                                   | 1127        | *****                                 | ****                                   | *****                                         | *****                                                         |                                                  | *****<br>*****                          | *****                                   | *****                                              | <br>:::::                 | * * * * * * * * * * * * * * * * * * *     | 11111                                   | *****                                   | *****                                   | *****       | :::::                                   | 11111                                                |
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|               |                                       |       |                                         |             |                                       |                                        |                                               |                                                               |                                                  |                                         |                                         |                                                    |                           |                                           |                                         |                                         |                                         |             |                                         |                                                      |
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| 2333          | * * * * * * * *                       | 11111 | 11111                                   | 71844       | 11211                                 | SETAR                                  | 4 4 5 9 6                                     | 11111                                                         | FEETE                                            |                                         | I TITE                                  | 11111                                              | 11111                     |                                           | ETCET                                   |                                         |                                         | TITTE       |                                         | 2 2 2 2 2                                            |
|               | * * * * * * * * * * * * * * * * * * * | ***** | * 1 * * * * * * * * * * * * * * * * * * |             | # # # # # # # # # # # # # # # # # # # | F +                                    |                                               | 4 4 4 4 7<br>4 4 4 4 7<br>4 4 4 4 8                           | 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4            | 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4   | 11 T T T T T T T T T T T T T T T T T T  | * * * * * * *                                      | 7 7 7 7 7                 | # ## ##<br># ####<br># #####<br># #####   |                                         |                                         | 7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | *****       | 2222                                    |                                                      |
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| + 22 52 52<br>1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 9 4 - 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4               | 1111 1E                                   | *** FFS.5                                                                 | * * * * * * * * * * * * * * * * * * * | E E E E E<br>E O V 7 9<br>E E E E E E     | ****                                    | * E ! E                   | E                                     | * * * * * * * * * * * * * * * * * * *   | 1 1 1 7 X                                                               | E 0.0.7 E                                          |                                                  |                                                        | 2000      | *****                   | 5055                                    | 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7        |
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| * 107 F 107  | 8                                                     | # K E W K O                               | ** * * * * * * * * * * * * * * * * * *                                    | * ****                                | T T T T T T T T T T T T T T T T T T T     | *****                                   | 5,5555                    | T T T T T T                           | F * C * C                               | 11446                                                                   | *****                                              | * * * * * * * * * * * * * * * * * * * *          | 2 0 0 4 4 4<br>2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 52000     | ****                    |                                         |                                                |
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SECTION 7

TABLE OF INTEGRATED ABSORPTANCE

Values of the integrated absorptance are presented in Table 7-1 for the samples which are listed in Table 4-1 and whose spectra and tables of transmittance are included in Sections 5 and 6, respectively. Except for wavenumbers near the ends of the spectral region of interest, all the tabulations for a given spectral interval are contained on two successive pages. A single page was sufficient to contain all the tabulations for the samples considered near the ends of the spectral region covered by the table.

The lower limit of integration ν^1 , which is shown at the top of each column, was chosen at a point where there was essentially no absorption. The integrated absorptance between any two wavenumbers listed can be found by subtracting the values tabulated at the two points. The accuracy of a given value of the integrated absorptance does not justify all of the significant figures which are carried in the table. But all these figures must be retained in order to avoid losing information about the integrated absorptance over narrow intervals which is obtained by subtracting the tabulated values. The table was formed by photographing part of the computer output with the proper headings pieced in above each section.

The integrated absorptance at a given ν was calculated by the computer from the values of transmittance given in Table 6-1 by the following expression.

$$\int_{V}^{V} \left[1 - T(v) \right] dv = \begin{bmatrix} v \\ \Sigma \\ v = v \end{bmatrix} \begin{bmatrix} 1 - T(v) \end{bmatrix} \Delta v \end{bmatrix} - \underbrace{\begin{bmatrix} 1 - T(v^{1}) \end{bmatrix} + \begin{bmatrix} 1 - T(v) \end{bmatrix}}_{2} \Delta v,$$

where $\Delta v = 0.1$ cm⁻¹, the wavenumber interval between successive values of T(v) in Table 6-1.

The important sample parameters are listed at the heading of each page.

In regions where the structure in the spectra is regular, the integrated absorptance was calculated at wavenumbers midway between the line centers. Therefore, in the case of no overlapping, the difference between two successive tabulated values is the equivalent width of the absorption line in the interval. In some other regions where the structure was not particularly regular, the integrated absorptance was calculated at wavenumbers corresponding to absorptance minima. In still other regions where there was but little structure or where the absorptance minima would shift as the pressure or absorber thickness was changed, the values were calculated at integral wavenumbers or possibly at integral half-wavenumbers, depending on the amount of information one might expect to obtain from closer readings.

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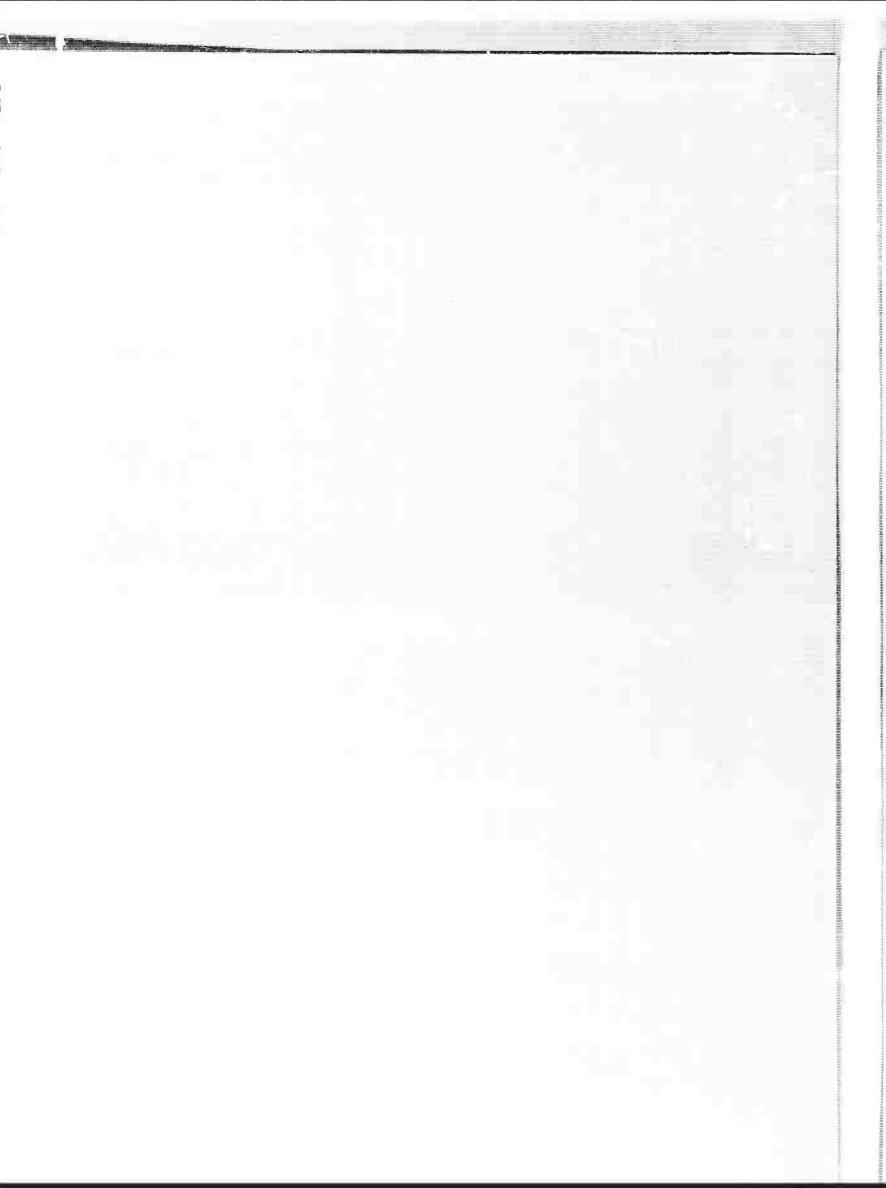
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SECTION 8

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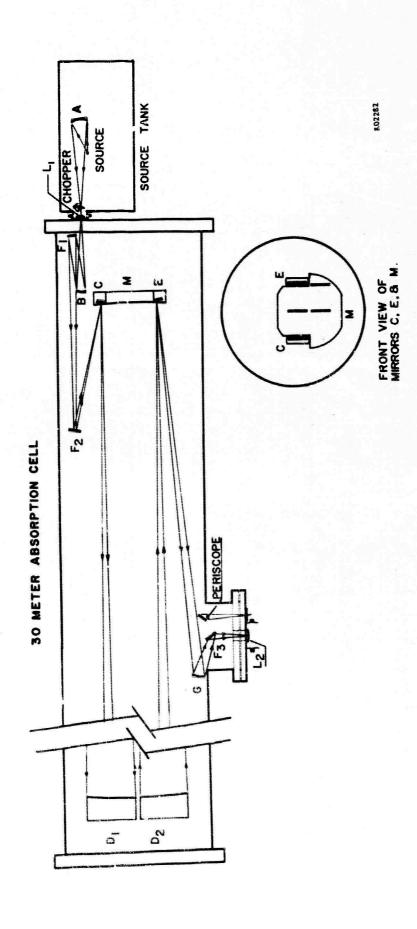


APPENDIX A

30-METER MULTIPLE-PASS CELL AND SOURCE TANK

Figure A-1 shows an optical diagram of a multiple-pass absorption cell with a base length of approximately 30 meters and an adjoining vacuum tank which contains a radiation source, chopper and mirrors. Light from a source is focused by mirror A on field lens L1 which serves as a window. From there the light passes on to mirror B which forms an enlarged image of the source on mirror C. The light then passes through the multiple-pass optical system which is of the type described by White (J. Opt. Soc. Am. 32, 285 (1942)). After traversing the multiple-pass system a certain number of times, which depends on the settings of mirrors D_1 and D_2 , an image of the source is formed on mirror E. The light then is directed to mirror G which re-images the source on field lens L2, which also serves as the exit window. From here the radiation is focused on the entrance slit of one of two spectrometers which are available in the laboratory. F1, F2 and F3 represent flat mirrors, and all mirrors are front surface aluminized.

The principle of the White multiple-pass system can be explained with the aid of the lower portion of Figure 1, which shows a front view of mirrors C, E and M, with the positions of the images shown on M when the system is adjusted for 8 passes. Light from the image on C travels to D1 whose radius of curvature is equal to the distance between M and D1; from there the light is reflected to form the lower right-hand image on M. M is a spherical mirror whose radius of curvature is, like D_1 and D_2 , equal to the distance (29.0 meters) between M and D₁ or D₂. The center of curvature of M is mid-way between D_1 and \bar{D}_2 ; therefore, all the light from the lower right-hand image falls on D2, which re-focuses the beam to the image in the upper center portion of M. The light then goes to D1 and to the lower left image on M, on to D2 and back to E, from where it is directed to G and out of the cell. The optical path from L_1 to C and from E to L_2 is 5 meters; therefore the total path inside the cell is 5 + 29 N meters, where N is the number of passes.



OPTICAL DIAGRAM OF THE 30-METER MULTIPLE-PASS ABSORPTION CELL AND SOURCE TANK FIGURE A-1. R02282

The lower portion shows a front view of mirrors C, E and M with the image pattern corresponding to 8 passes; the images are approximately 15 by 1.2 cm. The distance from M to D_1 and D2 is 29 meters. The number of passes of the beam before it strikes E is changed by rotating D_2 about a vertical axis. In many cells of this type, the number of passes is varied by moving both D_1 and D_2 ; however, it is only necessary to move one. D_1 and D_2 are D-shaped, both having been cut from a single mirror of 81 cm diameter, rather than from two circular mirrors, in order to obtain the maximum possible light gathering power with the 91 cm diameter tube in which the optics are installed. M is cut from a 46 cm diameter mirror.

Since the f-ratio of the multiple-pass system is large (approximately 75), it is necessary to use large images on C, E and M and to reduce them to the height of the entrance slit of the spectrometer in order to fill it properly. The images on C, E and M are approximately 15 cm high x 1.2 cm wide and are reduced to about 3.0 cm high at lens L_2 . The image is further reduced by optics outside the cell to match the height of the entrance slit of the spectrometer being used. The entrance optics work in just the opposite manner; an enlarged image of the source is formed at L_1 , and this image is further enlarged and formed on C. Mirrors B and G are similar, as are C and E.

Vignetting is avoided by using lenses L_1 and L_2 instead of flat windows and by using spherical mirrors C and E, rather than flats as is frequently done. Lens L_1 images mirror A on B; and C images B on D_1 . Similarly, E images D_2 on G, which is imaged on another mirror that is outside the cell, but not shown in Figure A-1. The need for curved mirrors C and E, rather than flats, and for lenses L_1 and L_2 is not apparent from Figure 1, which shows only the rays in a horizontal plane. However, the need is clear when one considers the height of the images on C, E and M. For example, if C were replaced by a flat mirror, the necessary height of the beam at B in order for light to go from every point on the 15 cm high image to every usable point on D_1 is approximately 20 cm. The maximum height of the portion of D_1 which is used is about 60 cm, and the optical distance from B to C is approximately 210 cm, thus the height of the beam on B is only about

$$60 \times \frac{210}{2900} \cong 4.4 \text{ cm}$$

when C is used with B and D_1 at conjugate points. Similarly, if L_1 were a plane window, the necessary height of the beam at A would be much greater. A similar argument applies for E and lens L_2 .

The loss that would arise from a slight error in the focal lengths of L_1 and L_2 is small; therefore, loss due to chromatic aberrations in the two lenses is negligible. The lenses, which are made from KBr, were ground to have the proper focal length for an intermediate wavelength of 3μ , so that the system can be used satisfactorily from the visible to 25μ . Since the f-ratio of the beam inside the cell is large and the reflections at B, C. E and G are nearly normal, these mirrors can be spherical without introducing a significant amount of aberration.

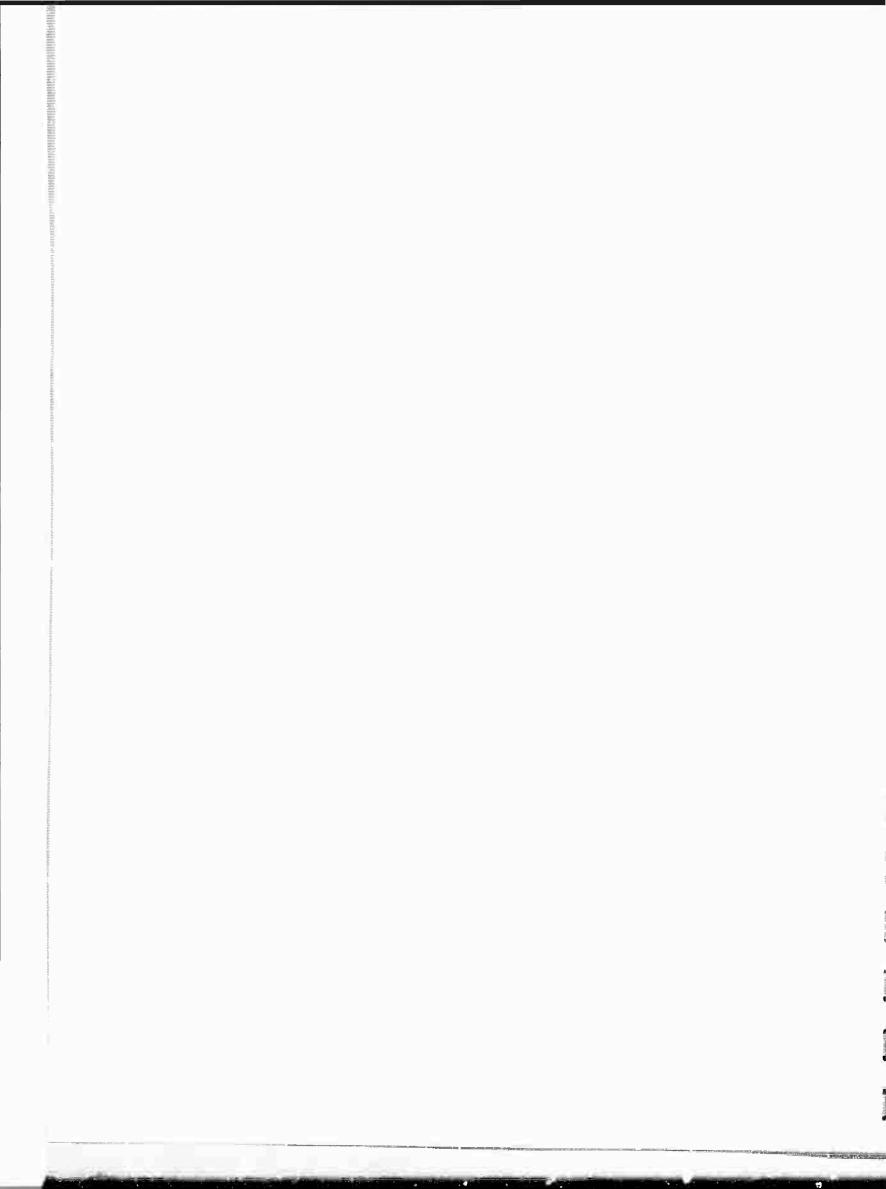
The front of M can be viewed through a small window and a flat mirror which is labelled as a periscope in Figure A-1. In this manner, it is possible to see the images on M and to determine the number of passe to which the system has been adjusted. Vertical and azimuthal adjustments can be made on both D_1 and D_2 from outside the cell by means of rotary seals. The adjustments on D_1 are used to position the first image on M; and the vertical adjustment on D_2 is used to place the centers of curvature of D_1 and D_2 at the same height. The azimuthal adjustment on D_2 is much finer and is used to change the number of passes.

The long cell is provided with a two-stage mechanical pump which is capable of attaining a pressure of a few tenths of a micron of Hg. The maximum pressure which can be used safely is about 2.5 atmospheres. Pressures are measured by a McLeod gauge, an oil manometer or an Hg manometer, depending on the pressure range. Electrical heating wire and insulation have been installed so that it is possible to heat the cell to approximately 70°C. Two fans inside the cell provide mixing when samples consisting of two or more gases are used.

It should be noted that the absorption cell was designed around the long pipe which was installed in the basement of the building as it was being erected before the authors were employed by Aeronutronic. For this reason, some of the things about the cell are not as they would be if the tube had not been previously installed. The cell could be improved somewhat if it were made of glass-lineo steel or of stainless steel which could be honed to provide a very smooth inner surface. With either of these surfaces the adsorption of gases, particularly H2O, on the walls would be less troublesome than with the rough steel walls which were used. It would also be more desirable if the cell were somewhat smaller and designed to hold higher pressures. If it were smaller, it would also be more practical to cool it to temperatures corresponding to the upper atmosphere.

The source tank is constructed of steel pipe having a 45 cm diameter and 6 mm wall thickness. A steel plate which has been welded in position approximately 8 cm below the horizontal diameter provides

a surface for mounting a chopper, a radiation source and mirrors. The tank can be connected to the long cell by the use of flexible bellows and can be evacuated to avoid errors due to absorption by atmospheric gases. The interior of the tank can be viewed through a window in the end plate farthest from the absorption cell. Small adjustments on mirror A, or on any other mirror which might be used, can be made from the exterior by the use of a rotating vacuum seal.



APPENDIX B

ONE-METER MULTIPLE-PASS ABSORPTION CELL

A shorter multiple-pass absorption cell has been constructed to supplement the 30-meter one in our laboratory. The shorter one, like the long one, has multiple-pass otpics using the principle described by White (J. Opt. Soc. Am. 32, 285 (1942)), with two mirrors at one end and a single mirror at the other end where the radiation enters and exits. The distance between the mirrors is 102.7 cm; and with an additional 4.8 cm ath jrside the cell, the total path for N passes is

L(cm) = 4.8 + N (102.).

Each of the two mirrors at the end opposite the windows has a useful area approximately 6 cm x 6 cm. Plano-convex lenses serve as windows to reduce vignetting. The height of the image at the single mirror is limited by the windows to approximately 4.5 cm. By means of a relatively simple set of mirrors, the image size can be reduced and the divergence of the beam increased in order to properly fill either of our monochromators, a Perkin-Elmer Model 99 or a "home-made" one utilizing a grating. The mirrors in the cell are coated with gold, rather than aluminum, because of the higher reflectivity of gold between 0.7 and 2 microns. In order to change the number of passes, the two mirrors at one end are rotated about vertical axes. This is accomplished by the use of a screw having left-hand threads on one end and right-hand threads on the other; the nuts are spring loaded against arms which extend approximately 70 cm in front of each mirror. The screw is coupled to an external crank through a rotating seal so that the number of passes can be changed without opening the cell or changing the sample.

A flat mirror mounted just below a small window in the top of the cell makes it possible to view the images on the single mirror near the windows. The number of passes can be determined from the image pattern.

The end of the cell containing the windows is fitted to a tlexible bellows which is joined to a vacuum tank containing the remainder of the optics. Therefore, it is possible to essentially eliminate absorption by atmospheric gases outside of the cell.

a Amir The cell is constructed from a piece of stainless steel pipe 120 cm long with an I.D. of 15 cm. The inside of the pipe is honed to provide a smooth surface and reduce adsorption of gases on the wall. All of the mirror mounts are also made of stainless steel so that many gases which would corrode other metals can be studied.

The entire cell is wrapped with heating coils and insulation so that it can be heated to approximately 170°C. A separate heating circuit is supplied for each end plate and one for the main body of the cell; still another circuit supplies extra heat in the regions of the valves and thermocouple wells which would otherwise be cooler than the remainder of the cell. The resistance wire with asbestos insulation was threaded through copper tubing which was then wrapped around the cell and soft-soldered to it to provide a good thermal contact. Three thermocouples at different locations inside the cell make it possible to measure the temperature so that the power to each heater can be adjusted for a uniform temperature.

The cell can also be cooled by putting it in an insulated tub which was designed for the cell and can be filled with dry-ice, ice water or any other desired cooling material so that the cell is completely immersed in it. In most of the measurements which are anticipated, it will not be necessary to attain an exact temperature; therefore, a continuous temperature control is not essential. Dry-ice or ice water as refrigerants have the advantage that the temperature is self-controlled. Some temperatures between those of these two materials can probably be attained by using frozen mixtures of water and alcohol. At the present time, the cell has not been used at reduced temperatures.

APPENDIX C

DATA DIGITIZING SYSTEM

I INTRODUCTION

A system for analysis and presentation of spectrographic data has been developed. This system performs the following:

- (1) The output of the spectrometer consisting of pen deflection as a function of prism or grating positions can be presented directly in digital form as pairs of numbers displayed on lamp bank indicators and punched and printed on standard IBM cards.
- (2) One can take the original strip charts, make any corrections to account for the presence of any unwarted gas or impurities and fit in the appropriate background curve (the curve giving the pen deflection with the sample removed). These corrected data can be both replotted and digitized as percent deflection vs. grating or prism position. The digital values again are displayed and punched on standard IBM cards. This freedom to correct, modify and study a number of strip charts (each perhaps representative of the same phenomenon with some systematic change in some parameter of the experiment) before the material is digitized is extremely convenient and desirable.

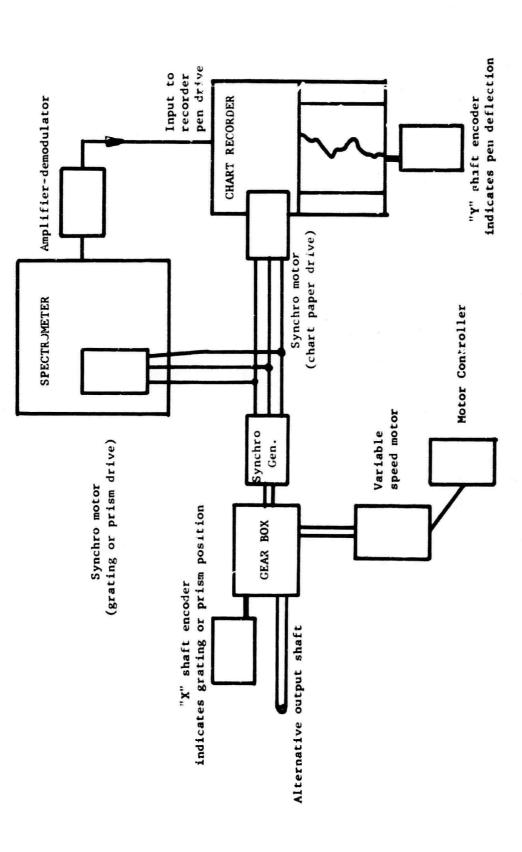
The pairs of data points can be taken at a rate slightly faster than one per second.

We will describe the system and its two basic modes of application in the following section.

II DESCRIPTION

a. The Direct Digitizing System

Figure C-1 shows the direct digitizing system. The spectrometer's prism or grating position, the chart advance of the strip chart recorder, and the X Shaft Encoder are driven directly or through "synchros" by a variable speed motor enabling one to match their speed to the nature of the spectrum. The slowest speed and the maximum density of recorded data points are selected to accurately present the spectrum in those regions where it is most complicated. By increasing the speed and/or reducing the density of recorded data points one can significantly reduce the total time required to cover the spectrum without loss of resolution. The gear ratios on the gear box are selected to establish the density of points derived from the



RO9911 FIGURE C-1. DIRECT DIGITIZING SYSTEM

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X Shaft Encoder indicating the position of the grating or prism; the number of these points which are actually recorded is controlled by the Readout Control device described below. The electrical output of the spectrometer is amplified, demodulated, and applied to the chart recorder pen drive. The resulting pen deflection is measured by the Y Shaft Encoder. The outputs of the shaft encoders go to the data processor subsystem.

b. The Digitizer and Data Processor Subsystem

This subsystem was designed and manufactured by Coleman Electronic Systems, Santa Ana, California, to our specifications. It consists of the following:

(1) Shaft Encoders

Two shaft encoders are used. They indicate the angular position of their input shaft in terms of contact positions of ganged rotary switches. The one mounted on a chart recorder measures pen deflection in units 0000 to 1,000. The second encoder synchronized with the chart paper drive measures the distance along the chart paper in units 00000 to 99,999.

(2) Data Processor

On command for readout the Gata processor unit translates the contact positions of the shaft encoder into contact closures of several banks of relays. These contact closures are presented in two forms: as a visual, numerical display on a lamp bank; and as an output to drive an IBM summary punch.

(3) Readout Control

The density of recorded data points can be adjusted so that a readout cycle is initiated with each change of 1, 2, 5 or 10 units of the X Shaft Encoder. This enables one to increase the number of points in those regions where the spectrum is complicated.

(4) Summary Punch Control

This device samples the data stored in the data processor during the readout cycle in a sequence and form compatible with an IBM 526 Summary Punch which records the data on standard IBM cards. In addition,

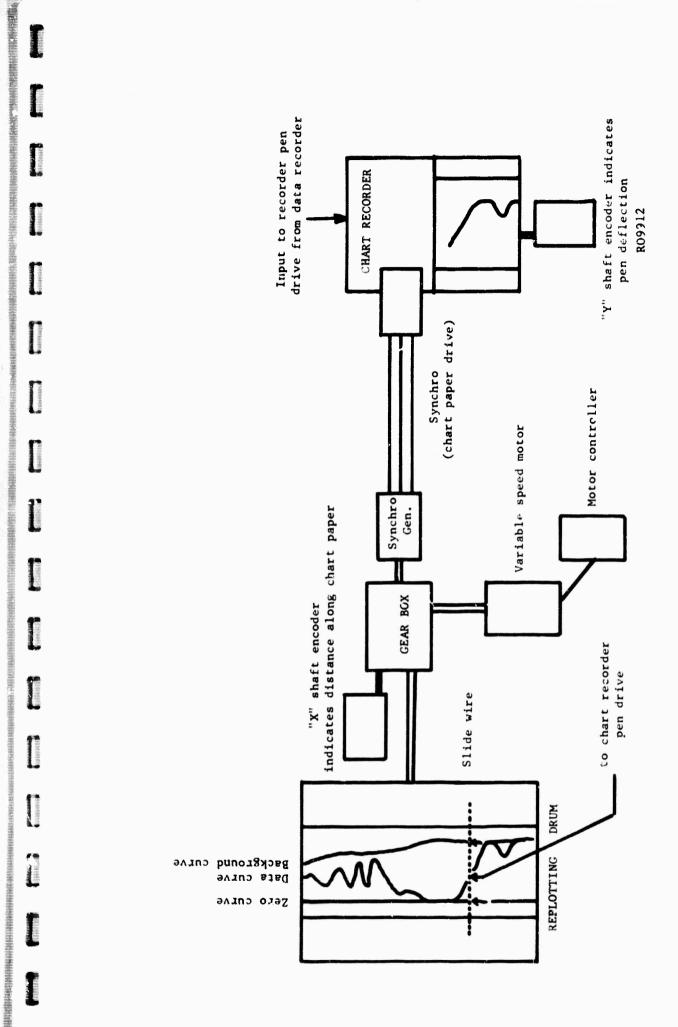
it provides for interlocking controls so that each punching sequence is completed before the following readout cycle can be initiated. The 80 columns of the IBM card can be used as convenient for recording the pairs of data points and any identifying code symbols. We have chosen to record seven pairs of data points and a five digit number to identify the spectrum on each card.

c. The Replotting and Digitizing System

Figure C-2 shows a modification of the direct digitizing system whereby the data previously recorded on strip charts can be digitized. In addition, if a zero level curve and a background curve are also recorded on the strip chart, the percent that the data curve is of the background curve can be digitized and replotted. The background curve corresponds to full scale; for example, in a simple transmission spectrum measurement of some sample it shows the spectrometer's output with the sample removed. In this application the alternative output shaft of the gear box drives a drum onto which is placed the strip chart which is to be digitized. This drum thus rotates in synchronism with the chart paper drive of the chart recorder and with the X Shaft Encoder. On a carriage mounted over the drum are three pointers which are tied to slide contacts along a slide wire-one for the background curve, one for the data curve and one for the zero level curve. A constant voltage corresponding to full scale deflection on the chart recorder is applied between the zero level slide contact and the background curve contact. The voltage from the data curve and the zero level contact thus give a measure of the percent deflection. Except to compensate for small drifts in the spectrometer characteristics, the zero point does not need to be adjusted. The data curve pointer is manually adjusted to follow the data curve; and through the use of two photodetectors in a bridge circuit and a servo system, the background pointer automatically follows the background curve.

III SUMMARY

We have described a very useful tool for the presentation and analysis of spectrographic data. The data can be directly digitized as it is being recorded or can be taken from strip chart records after corrections or modifications have been made. In addition, the percentage that a deflection shown on a strip chart is of some background curve can be recorded digitally and replotted. The output in the form of IBM punch cards enables the data to be conveniently introduced into a computer for additional analysis.



RO9912 FIGURE C-2. REPLOTTING AND DIGITIZING SYSTEM

PHILCO CORPORATION

A SUBSIDIARY OF Ford Company.

AERONUTRONIC DIVISION FORE ROAD/NEWPORT BEACH, CALIFORNIA

January 28, 1965

Please find enclosed the corrected copy of page 3-5 for Report U-2955 entitled "Scientific Report - Absorption By CO₂ Between 4500 and 5400 cm⁻¹" dated 15 December 1964.

The strengths given for the bands under the sub-heading New Bands were all in error by a factor of 10^{-4} in the original report. Please make note in your copy or insert the attached corrected page.

Darrell E. Burch David A. Gryvnak Richard R. Patty

ARCHIVE COPY

Corrected Page 3-5 for Report #U-2955 entitled "Scientific Report - Absorption By CO₂ Between 4500 and 5400 cm⁻¹" by D.E. Burch, D.A. Gryvnak and R. R. Patty, dated 15 December 1964 - PHILCO, Aeronutronic Division

TABLE 3-2
BAND STRENGTHS

			∫K	(v)dy (atm ⁻¹	m cm) S'	TP.
Transition	na vo cm 1	P	Q	R	Total Band ^b	Total Band Weber et al ^C
		•	Major Bands		<u>.</u>	
04 ⁰ 1	4853.578	0.11	0.00	0.12	0.23	- 0.30
1201	4977.793	0.52	0.00	0.53	1.05	1.11
20 ⁰ 1	5099.619	0.15	0.00	0.18	0.33	0.47
			New Bands			
15 ¹ 0	4591.0	0.16x10 ⁻⁴	0.04×10^{-4}	0.22x10 ⁻⁴	0.42x10 ⁻⁴	
$06^{0}1 + 10^{0}0$ $30^{0}1 + 02^{2}0$	4587.75 5217.63	0.06×10 ⁻⁴	0.00x10 ⁻⁴	0.27×10 ⁻⁴		
02 ⁰ 2+01 ¹ 0	5248	0.09×10^{-4}	0.17×10^{-4}	0.07×10^{-4}	0.33x10 ⁻⁴	
10 ⁰ 2 01 ¹ 0	5349	0.03×10^{-4}	0.08×10^{-4}	0.03×10^{-4}	0.14×10^{-4}	

^aAll bands listed in this Table pertain to the $C^{12}O_2^{16}$ molecule.

The uncertainty in the values for the major bands is about six or eight percent, but it is considerably higher for the new bands.

CValues are taken from Weber, Holm and Penner and multiplied by 300/273 to adjust to density at STP. The authors give an uncertainty of 20%.

The strengths of the new bands were determined from our raw spectra by Benedict 9 .